Yakima River Basin Study

Modeling of Reliability and Flows Technical Memorandum

U.S. Bureau of Reclamation Contract No. 08CA10677A ID/IQ, Task 6

Prepared by

HDR Engineering, Inc Anchor QEA



U.S. Department of the Interior Bureau of Reclamation Pacific Northwest Region Columbia-Cascades Area Office



State of Washington Department of Ecology Office of Columbia River

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1.0 Introduction

The purpose of this memorandum is to document the development of the RiverWare model and results used in the Yakima Basin Study. The Yakima Basin Study will result in an Integrated Water Resources Development Plan for meeting the instream and out-of-stream needs for current and future water supply associated with the Yakima River system. The model of the system (YAKRW) is being used to estimate the specific effects of proposed new water resources projects on water supply and instream flow conditions. It is also being used to estimate the effects of potential climate change on future water supplies and instream flows.

The RiverWare software was developed by the Center for Advanced Decision Support for Water and Environmental Systems at the University of Colorado. The YAKRW model of the Yakima Basin (which uses the RiverWare software) was originally developed for the Yakima Field Office to evaluate seasonal operations strategies, it was adapted for use as part of the Yakima River Basin Storage Assessment Appraisal Study, completed from 2006 through 2008. It was further updated in 2009 and 2010 to represent current operations practices for use in the Columbia Basin River Management Joint Operations Committee (RMJOC) studies. The specific version of the model used in this study was obtained from Reclamation's Technical Service Center (TSC) in the spring/summer of 2010, where it had been modified slightly for use in evaluating the effects of potential climate change. HDR Engineering, Inc. further modified this TSC model to incorporate the planned water conservation measures and water demand increases anticipated for the basin. This model was used to estimate water supplies, stream flows, and reservoir levels associated with a scenario titled "Future without Integrated Plan" (FWIP).

A second scenario was then developed by including six proposed projects considered for inclusion in the Integrated Plan – Kachess to Keechelus Pipeline, Kachess Inactive Storage, Wymer Offstream Storage, Bumping Reservoir Enlargement, Enhanced Water Conservation, and Groundwater Infiltration. A Non-Storage Scenario (that included only the Enhanced Conservation and Infiltration projects) was also evaluated. Finally, the FWIP and Integrated Plan scenarios were evaluated under the estimated hydrologic impacts associated with three different climate change assumptions.

The YAKRW model provides a massive amount of output related to daily time-step stream flows, water levels, and water deliveries in the Yakima Basin. For this analysis, four primary metrics were used to summarize and compare modeled scenarios. These include:

- Total water supply available (TWSA), which is a combined measure of available water in streams and reservoirs
- Prorationing, which represents the percent of a given year's supply that is available to the proratable water right holders, who may have their supplies cut in low supply years
- April through September deliveries, which sums the total volume of water delivered to water users during the critical demand period
- End of September reservoir storage, which shows how much additional water is available to be carried over to next year at the end of the water year (the effective end of the irrigation season is October 20).

A fifth metric (a comparison between instream flow target levels and modeled stream flow in 15 critical reaches throughout the basin) was also used to evaluate results and impacts, although not as a simple, single metric. Instead, instream flow under scenario conditions is summarized in a matrix and on map-based figures.

The following sections briefly describe the Yakima Basin, the development of the model used in this study, and the assumptions used in each of the three modeled scenarios (FWIP, Integrated Plan and Non-

Storage). This is followed by the results from the simulation of the three scenarios and from several adjusted scenarios. The adjusted scenarios are based on a modified Integrated Plan that excludes one of the three major proposed storage projects (Kachess, Wymer, or Bumping). These adjusted scenarios were evaluated to show the effectiveness of the Integrated Plan if one of the large storage projects is not completed. Finally, results from the Integrated Plan and FWIP scenarios are presented under climate-impacted conditions.

2.0 Basin and Model Description

This section summarizes the Yakima Basin and major irrigation districts, the key components of the YAKRW model, the process of developing the scenarios used in this study, including stakeholder input, and a summary of the significant revisions to the model inputs used in generating the scenarios and their results.

2.1 YAKRW Sub-Basins and Irrigation Districts

Figure 1 shows a map of the Yakima River Basin, including the major proposed projects considered in the Integrated Plan. Figures 2 and 3 provide a schematic representation of inflows and diversions modeled in YAKRW along the mainstem of the Yakima River. For this memo, the basin is divided into several geographic areas. The upper Yakima contains three water supply lakes: Keechelus Lake, Kachess Lake, and Cle Elum Lake. Downstream on the Yakima River, several diversions take water for irrigation and municipal and industrial (M&I) uses in the Kittitas Reclamation District (KRD). The Naches River, a major tributary to the Yakima River, has two reservoirs (Rimrock and Bumping) that deliver water to several irrigation districts in the lower Naches River area. The Naches River joins the Yakima River near the city of Yakima, and marks the boundary between the upper and lower Yakima.

In the lower Yakima River area, several major canals, including the Roza, Sunnyside, and Wapato, supply multiple irrigation districts. The United States Geological Survey (USGS) gaging station on the Yakima River at Parker is a key flow indicator location where target flows are defined. The last area of interest is the Yakima River near the Columbia River. The Chandler power plant generates energy from run-of-river flows. Several smaller irrigation districts, Kennewick, Columbia, and Kiona, are also located in the lower Yakima River area.

Kittitas Reclamation District

The KRD area is on the upper Yakima River between Easton and the head of the Yakima Canyon. Lakes Keechelus and Kachess flow into Lake Easton, which serves as the diversion point for the KRD Main Canal. The KRD Main Canal splits into the South Branch Canal and North Branch Canal; the latter passes via siphon under the Yakima River. The South Branch Canal serves three irrigation areas in the model, before flowing into Long Tom Creek.

Several other canals in the Kittitas Valley divert downstream of Lake Easton. These include the Cascade Canal (which has separate gravity and pumped diversions), the West Side Canal, the Town Canal, and Ellensburg Power Canal. Flows can be diverted from the North Branch to the Cascade Canal and Town Canal. The Taneum Canal diverts from Taneum Creek, a tributary of the Yakima.

Model schematics of the KRD canals are included in Appendix A.

Multiple direct diversions from the Yakima River are not supplied by KRD canals. These diversions include the City of Cle Elum M&I needs, Younger, O'Conner, Knoke, Mills and Son, Woldale, Ellensburg M&I, Ellensburg Mill and Feed, Bull Canal, Fogarty Dyer Canal, Vertrees Diversions 1 and 2, and Tjossem, and Stanfield canals.



Figure 1. Yakima Basin Study Area and Major Projects Included in the Integrated Plan

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Figure 2. Yakima River Mainstem Model Schematic



Figure 2. Yakima River Mainstem Model Schematic (cont.)

Naches River Basin

A schematic of the lower portion of the Naches River is provided in Figure 3. Bumping and Rimrock reservoirs are located in the upper basin. Two significant irrigation districts have diversions in the Naches basin; the Yakima-Tieton Irrigation District and the Naches Selah Irrigation District.

The following water use diversions are in this area:

- Anderson
- Emerick
- Nile Valley
- Carmack Parker
- Fredricks Hunting
- Stevens
- Naches Selah Canal
- Wapatox (irrigation and M&I components)
- Foster Naches
- Clark
- South Naches
- Kelly Lowry
- Yakima-Tieton Canal
- City of Yakima (irrigation and M&I components)
- Gleed
- Morrissey
- Congdon
- Chapman Nelson
- Naches Cowiche

Lower Yakima

Irrigation districts located in the lower Yakima area include the Roza Irrigation District, Sunnyside Valley Irrigation District, Selah & Moxee Irrigation District, Union Gap Irrigation District, Ahtanum Irrigation District, Grandview Irrigation District, and diversions for the Confederated Tribes and Bands of the Yakama Nation (Wapato Canal). The Benton Irrigation District is located off of the tail of the Sunnyside Canal. Model schematics for the lower Yakima canals are included in Appendix A.

The following points of diversion are located in this area:

•

• Roza Canal

Hubbard Canal

Boise Cascade CanalUnion

- Blue Slough Diversion
- Reservation, or Wapato, Canal

• Moxee Canal

• Taylor Diversion

Selah Moxee Canal

Richartz Diversion

Gap Canal

• Sunnyside Canal

The canals on the north side of the Yakima River, which include Roza, Selah Moxee, Moxee, Hubbard, and Sunnyside, provide return flows into several common wasteways. Return flow also enter s the wasteways from the south side of the Yakima River from the Yakima Nation drains. Portions of flows in the wasteways can be recaptured for irrigation.

Yakima River near Columbia Confluence

The area of the Yakima River near the confluence with the Columbia River has three irrigation districts – the Kiona, Kennewick, and Columbia. Appendix A contains the model schematics for these districts.

The Chandler Canal diverts flow from the Yakima River. The Chandler Canal bifurcates to allow operation of a hydropower plant, which discharges to the Yakima River. The remaining flow is used by the Kennewick Irrigation District; a portion goes to the canal while the other portion is used by hydro turbines to pump the water up to the KID canal. The hydro turbine water returns to the Yakima River at the Chandler power plant. KID's water is transmitted via siphon under the Yakima River to the Kennewick Main Canal, which does not receive water directly from the Yakima River.

Further downstream on the Yakima River are diversions for the Kiona, Columbia, and Richland canals. The latter two divert from the Horne Rapids diversion dam. The Columbia Canal runs parallel to the Yakima River on the south side, while the Richland Canal continues on the north side. The Richland canal also appears to be referred to as the Horne Rapids Ditch in U.S. Geological Survey (USGS) mapping.

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Figure 3. Naches River Model Schematic and Tieton River Model Schematic





Figure 3. Naches River Model Schematic and Tieton River Model Schematic (cont.)

2.2 YAKRW Description

Inflows

Reclamation provided five hydrologic inflow datasets, one natural flow dataset and four climate change data sets. The first is the primary dataset used in scenario analysis called "No Regulation No Irrigation" (NRNI). This dataset, known as a "naturalized dataset," is derived from USGS and Reclamation's Hydromet observed data and represents stream flows as they would have been if there were no reservoirs and no diversions from the system. The dataset consists of daily values representing historical hydrologic conditions from water years 1981 through 2005. This historically-based period of record was used to predict how the system will operate in the future with new facilities, new operational arrangements, and (in some scenarios) climate-impacted flows and water needs. The remaining four datasets were provided by Reclamation's Technical Service Center (TSC) in Denver for climate change analysis. These datasets are described in the "Climate Change" section.

The following inflow locations (including specific tributaries and local inflows) are used in the model:

Yakima River

- Inflows into reservoirs
- Big Creek
- Little Creek
- Dry Creek
- Manastash Creek
- Reecer Creek

- Taneum Creek
- Robinson Creek
- Cherry Creek
- Wilson Creek
- Wenas Creek
- Toppenish Creek

- Satus Creek
- Sulphur Creek
- Teanaway River
- Swauk Creek
- Little Naches River
- American River

- **Naches River**
 - Inflows into reservoirs
 - Milk Creek
 - Swamp Creek
 - Devil Creek
 - Lost Creek

- Gold Creek
- Rock Creek
- Nile Creek
- Rattlesnake Creek
- Oak Creek

- Cowiche Creek
- Tieton River
- Little Naches River
- American River

Additional tributaries not included in the lists above are also used in the model and can be seen in Figures 2 and 3.

Reservoir Operations and Target Flows

For modeling purposes, reservoir releases are generally composed of:

- Flood releases to follow flood control space guidelines, at times based on forecasting¹
- Water supply for irrigation and M&I releases, including canal losses
- Augmentation for demand shortages generated by other reservoirs failing to meet their scheduled demand releases due to other overriding constraints
- Target flows at each reservoir outfall and Reclamation gages at Easton, below Tieton Canal, Naches, and Parker (EASW, TICW, NACW, and PARW)

¹ The model implements this and other types of forecasting that do not incorporate any forecasting error, thus generating a "perfect knowledge forecast". A TSC study using the Yakima model indicated negligible differences when forecasting error was introduced.

Instream flow targets generally vary by available storage in the reservoirs and hydrologic condition of a given year. Using a table provided by Reclamation, the model forecasts the September 1 storage in each reservoir based on inflows and anticipated demand releases. The El Niño/La Niña-Southern Oscillation (ENSO) index is included in the model and used to determine whether the year is more likely to have below average, average, or above average runoff. Based on ENSO and forecasted storage, the model selects a dry or average instream target dataset.

Table 1 lists the range of instream flow targets. The Parker (PARW) target is described in more detail in Section 2.2.3. These existing instream flow targets are applied to the baseline FWIP and Non-Storage scenarios. The Integrated Plan uses augmented instream flow targets described in Section 2.2.5.

LOCATION	RANGE OF INSTREAM FLOW TARGETS (CUBIC FEET PER SECOND)
Keechelus Reservoir	80 to 100
Kachess Reservoir	15
Cle Elum Reservoir	180 to 220
Rimrock Reservoir	45 to 100
Bumping Reservoir ¹	0 to 130, with 600 to 900 cfs peak flows in summer
Yakima River at Easton (EASW)	190 to 220
Tieton River	50
Yakima River near Parker (PARW) ²	300 to 600

¹ Bumping Reservoir instream flow target is a function of current Bumping storage and TWSA.

² PARW instream flow target is a function of the TWSA index, described in Section 2.2.5.

Existing reservoir operations are governed by what is called "flip-flop" operations, which serve to meet water supply demands while balancing fishery lifecycle needs. These operations are as follows:

During early spring and mid-summer, Yakima River mainstem demands are primarily met through releases from the three upper Yakima River reservoirs. The two Naches River system reservoirs will release flows to meet Naches system demands; Bumping Reservoir will release flows to meet upper Naches demands; and Rimrock Reservoir releases for Tieton and lower Naches demands.

Beginning in late August, the Yakima River mainstem demands will "flip-flop" from the upper Yakima reservoirs to the Naches system reservoirs. Demand releases from upper Yakima reservoirs are reduced to meet KRD system demands and upper river instream flow targets. Rimrock releases are applied to meet Yakima mainstem demands and the instream flow target at Parker. The goal of this operation is to target upper Yakima River stages during the spawning period at roughly the same levels that will be targeted during the winter. Chinook salmon and other anadromous species will construct their nests below the river's water surface. The eggs will suffer higher mortality if the river stage falls after spawning and exposes the eggs. A "mini-flip flop" operation also takes placed between Keechelus and Kachess reservoirs to supply KRD demands and reduced flows in the Yakima River between Keechelus and Lake Easton.

Table 2 shows the initial reservoir storage quantities used for the simulation period. These quantities correspond to historic storages on October 1, 1980, the start date of the simulation period. These storage levels are also typical for this time of year, so should adequately represent initial conditions without imparting a bias to the results.

Lake Easton is a reregulating reservoir that maintains a constant pool elevation of 2,180.33 feet, which corresponds to 3,999 acre-feet. There is no simulation of precipitation, evaporation, or seepage from any

of the reservoirs in the model because these factors are assumed to be incorporated into the natural flow determination used in the original development of the hydrology.

RESERVOIR	INITIAL STORAGE (ACRE-FEET)	% OF CAPACITY
Keechelus Lake	18,982	12%
Kachess Lake	90,641	38%
Cle Elum Lake	23,934	5%
Lake Easton	3,999	100%
Bumping Reservoir	4,839	14%
Rimrock Reservoir	44,493	22%

Table	2. Initial	Reservoir	Storage
-------	------------	-----------	---------

Modeling of Demands and Groundwater Storage

RiverWare is an "object-oriented" modeling tool. This means that it uses graphical "objects" to represent features of the simulated system. These objects can be river reaches, reservoirs, groundwater elements, etc., and frequently include detailed functions that describe their operations. Figure 4 shows a generic schematic of canal and water use in the model. A generic "main canal" object diverts flow from a river for all associated service areas. Each reach of the main canal can have seepage based on the rate of flow, which is transferred to a groundwater simulation object. Delivery laterals pull water from the main canal to a service area. A portion of flow becomes seepage and is transferred to the groundwater object. Water delivered to the service area is divided into consumptive use and return flows. A fixed portion of service area return flow is recharged to the groundwater object while the remainder is surface water returns to a river.

The groundwater simulation object implements a linear response function, which translates groundwater recharge into surface water impacts. A storage value is maintained by the object that represents the state of the aquifer. Impacts to a surface water body are calculated as a fraction of the groundwater storage. According to Reclamation (C. Lynch, personal communication) these groundwater parameters were based on trial-and-error in matching observed flows.

The initial storage of the groundwater object needs to be set to represent steady-state conditions. A groundwater object that is not initialized to a steady-state condition can artificially accumulate recharge or generate additional surface-water impacts. For example, setting the initial storage to a value of zero creates a condition where no irrigation-related aquifer recharge has occurred prior to starting the model run. During simulation, the aquifer accumulates recharge until the overall recharge and discharge balance. During the transition from no irrigation to an irrigated condition, discharge to the river is artificially low.

Setting the initial storage is a trial-and-error approach. An initial aquifer storage estimate is selected and then compared to the final simulated aquifer storage value. If the difference is greater than a specified difference, the initial storage is set to the final storage. The model is rerun until final and initial storages converge to within a given tolerance.



Figure 4. Generic Irrigation Model Schematic

Water Use Efficiencies

Water use efficiency is defined here as the portion of water diverted from a specific point that is applied for a consumptive beneficial use in a service area. Three components of efficiency are used in the model:

- 1. Efficiency of a main canal is the amount of water diverted from a river that arrives at a given lateral; seepage to the aquifer affects this efficiency value.
- 2. Efficiency of a delivery lateral is the portion of water reaching the lateral that is delivered to a use site (e.g., a field). Seepage losses along the delivery lateral will affect delivery efficiency.
- 3. Efficiency at the site of use is the consumptive portion of the delivery. This is affected by the quantity that runs off or seeps back into the groundwater system.

The overall efficiency, from the point of diversion on a river to a site of consumptive use, is the multiplication of the three component efficiencies listed above.

Table 3 lists the efficiencies for the water uses in the model in alphabetical order by irrigation district. Efficiency values were extracted from the Reclamation RiverWare model and expressed as a seepage loss as a function of flow. These efficiencies are increased during simulations incorporating conservation as the canal and other losses are decreased (see Table 6).

Demand Amounts

Estimates of the available water supply are described in the TWSA index. This index is calculated as the sum of the reservoir storage and the forecast of irrigation return flows and runoff below the reservoirs. Only a portion of the TWSA index is available to meet irrigation and M&I demands in a given year. A second index, Water Supply Available for Irrigation is calculated as TWSA minus the flow past the Parker gage (which includes excess natural flow and the instream flow targets at this downstream-most target location), minus the estimated September 30 reservoir carryover storage. The Parker instream flow target is a step-wise function of TWSA, as provided in Table 4. As TWSA increases, the instream

flow target increases in steps. The September 30 carryover storage is estimated in the model with the minimum value fixed at 85,000 acre-feet.

Proration is the method of shortage-sharing in the Yakima River Basin project. Irrigation systems have shares denoted as non-proratable or proratable. Non-proratable shares predate the Yakima Storage project and are considered to be within the firm yield of the system and are always supplied (although the model can proportionally reduce the non-proratable shares, if necessary, in severe drought years). The proratable shares have a priority date of May 5, 1905, and are above the firm yield and may be subject to proportional curtailment. A proration ratio is calculated based on the ratio of Water Supply Available for Irrigation in excess of the non-proratable shares divided by the total proratable shares but is capped at 1.0. A proration ratio of 1.0 indicates a full supply where all shares are fully satisfied. A lower ratio means that all proratable shares are curtailed by a given amount. For example, a proration ratio of 0.70 indicates that proratable shares will receive 70 percent of their nominal supply entitlement. The model however will assign a district's diversion amount based on the lesser of the prorated supply or their median accepted diversion for a non-drought (wet) year.

Irrigation diversions start no earlier than March 1 and end no later than October 31. The model converts annual values into daily values using a fixed daily pattern. Table 5 lists the average diversion values for dry and wet years for each demand along with the proportion of the demand that is proratable. These values were obtained from the Reclamation RiverWare model. The demand time series were developed by Reclamation based on observed canal flows.

For many water users, diversions are higher in wet years (even though demand may be lower) because water supply is greater. In some cases it is possible for the opposite to occur, with diversions higher in dry rather than wet years. In part, this happens because the "dry" and "wet" categories are based on TWSA, not the meteorological conditions occurring during the irrigation season.

FFFICIENCY					EFFICIEN	ICY			
	MAIN					MAIN			
LOCATION	CANAL	DELIVERY	SITE	OVERALL	LOCATION	CANAL	DELIVERY	SITE	OVERALL
Benton	n/a	85%	64%	54%		Ro			
	Cascade C	anal (pumped	l)		Diversion 1	99%	68%	64%	43%
Diversion 1	98%	58%	64%	36%	Diversion 2	96%	89%	64%	55%
Diversion 2	97%	80%	64%	50%	Diversion 3	91%	90%	64%	53%
Diversion 3	94%	82%	64%	49%	Diversion 4	83%	82%	64%	44%
Diversion 4	87%	86%	64%	48%	Diversion 5	81%	90%	64%	46%
	Chandle	r-Kennewick			Diversion 6	72%	89%	64%	41%
Diversion 1	45%	95%	64%	27%		Selah	Moxee		
Diversion 2	23%	95%	64%	14%	Diversion 1	98%	82%	64%	52%
Diversion 3	11%	95%	64%	7%	Diversion 2	88%	82%	64%	47%
	Colum	bia Canal			South Naches	n/a	30%	64%	19%
Diversion 1	50%	95%	64%	30%		Sunr	nyside		
Diversion 2	25%	95%	64%	15%	Diversion 3	98%	94%	64%	59%
	Ellensb	ourg Power			Diversion 4	92%	91%	64%	54%
Diversion 2	93%	82%	64%	49%	Diversion 5	87%	93%	64%	52%
Diversion 3	85%	82%	64%	45%	Diversion 6	81%	90%	64%	47%
Hubbard	90%	81%	64%	47%	Taneum Ditch	95%	75%	64%	46%
Kiona	n/a	95%	64%	61%	Tieton Canal				
	KRD No	orth Branch			Diversion 1	100%	99%	64%	63%
Diversion 1	97%	65%	52%	33%	Diversion 2	99%	99%	64%	62%
Diversion 2	96%	77%	52%	38%		Town	Canal		
Diversion 3	95%	78%	52%	39%	Diversion 1	100%	100%	64%	64%
Diversion 4	83%	84%	52%	36%	Diversion 2	100%	100%	64%	64%
	KRD So	uth Branch			Diversion 3	100%	100%	64%	64%
Diversion 1	94%	79%	52%	38%	Diversion 4	100%	100%	64%	64%
Diversion 2	89%	79%	52%	37%	Union Gap	90%	81%	64%	47%
Diversion 3	85%	81%	52%	36%	Wapatox	n/a	95%	64%	61%
Moxee	90%	82%	64%	47%		West Si	de Canal		
Naches Selah									
Canal	n/a	80%	64%	51%	Diversion 1	98%	82%	64%	52%
	Reservation	(Wapato) Car	nal		Diversion 2	96%	82%	64%	51%
Diversion 1	98%	84%	64%	53%	Diversion 3	87%	82%	64%	46%
					Small Irrigation				
Diversion 2	74%	72%	64%	34%	Diversions	n/a	75%	64%	48%
	Richla	ind Canal	1		M&I Diversions	n/a	100%	50%	50%
Diversion 1	95%	95%	64%	58%					
Diversion 2	90%	95%	64%	55%					
n/a = Not Availabl	e –								

Table 3. Water Use Efficiencies

MINIMUM TWSA	PARKER INSTREAM				
Month of April					
3,200,000	600				
2,900,000	500				
2,650,000	400				
0	300				
M	onth of May				
2,900,000	600				
2,650,000	500				
2,400,000	400				
0	300				
M	onth of June				
2,400,000	600				
2,200,000	500				
2,000,000	400				
0	300				
Months o	f July to September				
1,900,000	600				
1,700,000	500				
1,500,000	400				
0	300				
All other months	400				

Table 4. Yakima River at Parker Instream Flow Targets

The model assumes a wet year demand value for March. Between April 1 and September 30, either a wet year demand value or a prorated demand value can be used based on the hydrologic condition of a given year. If full water supply cannot be achieved, the October demand value is also based on prorationing. Each canal system has a unique pattern of demand. Figures 5 through 10 show the average daily pattern of total basin-wide proratable and non-proratable demand. In no case will the model use a value greater than what the wet year curve would indicate even if the proration rate times the entitlement would equal a greater value.



Figure 5. Kittitas Irrigation District Modeled Proratable and Non-Proratable Demand



Figure 6. Naches-Selah Irrigation District Modeled Proratable and Non-Proratable Demand



Figure 7. Roza Irrigation District Modeled Proratable and Non-Proratable Demand



Figure 8. Sunnyside Irrigation District Modeled Proratable and Non-Proratable Demand



Figure 9. Yakima-Tieton Irrigation District Modeled Proratable and Non-Proratable Demand



Figure 10. Westside Irrigation District Modeled Proratable and Non-Proratable Demand

	ANNUAL DIVERSION	S (ACRE-FEET/YEAR)						
CANAL LUCATION	DRY YEAR	WET YEAR	NON-PRORATABLE	PRORATABLE				
Irrigation Districts and Canals, including Hydropower Generation								
Anderson	239	250	100%	0%				
Benton Canal	16,173	18,400	69%	31%				
Blue Slough	646	675	100%	0%				
Boise Cascade	1,409	1,473	99%	1%				
Bull	1,327	1,315	100%	0%				
Cascade Pumps below Slide	6,907	6,841	100%	0%				
Carmack Parker	97	102	100%	0%				
Cascade Gravity	-	-						
Chapman Nelson	1,163	1,216	100%	0%				
Clark	694	726	100%	0%				
Cobb Upper	111	116	100%	0%				
Congdon	4,266	4,460	85%	15%				
Ellensburg Mill and Feed	985	976	100%	0%				
Ellensburg Power	1,237	1,225	100%	0%				
Ellensburg Town	9,795	9,702	100%	0%				
Emerick	105	109	100%	0%				
Fredricks Hunting	145	151	100%	0%				
Fogarty Dyer	757	750	100%	0%				
Foster Naches	230	240	100%	0%				
Fruitvale	2,695	2,818	100%	0%				
Gleed	3,473	3,631	100%	0%				
Hubbard	1,699	1,777	100%	0%				
Kelly Lowry	1,292	1,351	100%	0%				
Knoke	328	325	100%	0%				
KRD Main	232,455	334,489	0%	100%				
Mills and Son	1,544	1,530	100%	0%				
Morrissey	184	192	100%	0%				
Moxee	792	828	82%	18%				
Naches Cowiche	2,298	2,402	100%	0%				
New Reservation Canal	538,279	612,529	47%	53%				
Nile Valley	662	692	100%	0%				
O'Conner	636	630	100%	0%				
Old Reservation Canal	-	-						
Old Union	2,690	2,813	100%	0%				
Richartz	969	1,013	100%	0%				
Roza Canal	254,070	350,463	0%	100%				
Selah Moxee	4,836	5,056	87%	13%				
Sinclair	120	125	100%	0%				
South Naches	3,493	3,651	100%	0%				
Stanfield	328	325	100%	0%				

Table 5. Average Annual Diversions and Proratable Proportions

	ANNUAL DIVERSION	S (ACRE-FEET/YEAR)			
CANAL LUCATION	DRY YEAR	WET YEAR	NON-PROKATABLE	PRUKATABLE	
Stevens	297	310	100%	0%	
Sunnyside Canal	400,420	455,559	69%	31%	
Tieton Canal	86,984	92,752	67%	33%	
Tenant	239	250	100%	0%	
Tjossem	979	969	100%	0%	
Taylor	1,218	1,273	100%	0%	
Union Gap	3,849	4,024	82%	18%	
Vertrees 2	144	143	100%	0%	
Vertrees 1	444	440	100%	0%	
Wapatox Irrigation	3,079	3,219	100%	0%	
Woldale	2,661	2,635	100%	0%	
Younger	617	611	100%	0%	
Subtotal, Irrigation	1,600,060	1,937,552			
	Municipal	and Industrial (M&I) Us	ses		
City of Cle Elum M & I	258	256	100%	0%	
City of Ellensburg M & I	1,231	1,219	0%	100%	
City of Yakima M & I	1,424	1,489	52%	48%	
City of Yakima Irrigation	1,568	1,640	85%	15%	
Subtotal M&I	4,481	4,604			
Total	1,604,540	1,942,155			

Table	5. Average	Annual	Diversions	and	Proratable	Proportions	(cont.)
Table	J. Average	Annuai	Diversions	anu	Toracable	roportions	

Minor Deficiencies Identified in Model

Several apparent deficiencies were identified in reviewing the models provided by Reclamation. These items have been forwarded to Reclamation for consideration. They are considered to be relatively minor and did not require correction to run the model for overall purposes of the Yakima Basin Study. However some of these items may affect the precision of specific model outputs in the study. The apparent deficiencies include the following:

• Gold Creek and Cowiche Locations:

Gold Creek in the model flows into the Naches River below Lost Creek. Based on the USGS hydrographic map, Gold Creek is located upstream of Lost Creek. This difference may impact demands met at the Anderson Diversion location because it may indicate that the Anderson water right does not include Gold Creek.

• Reservoir Evaporation, Precipitation, and Seepage:

Evaporation, precipitation, and seepage for reservoirs are not simulated in the model, although historical effects were incorporated in the stream flows and reach gains and losses used in developing the model's hydrologic database. The lack of these reservoir water budget components will not impact scenario evaluation, except where new (or significantly enlarged) reservoirs are assumed, or reservoirs are operated much differently than under baseline conditions. Even then, effects are likely to be very small compared with the water volumes being considered in this study.

• Water Use Efficiencies:

Chandler-Kennewick Canal and Columbia Canal appear to have lined delivery canals but high seepage from the main canal. The main and delivery canals for Town Canal also appear to be lined. These items should be verified for scenarios considering water conservation.

• Groundwater Returns:

Several groundwater return flows are not linked to surface-water locations. This causes the groundwater returns to be consumptively used. This could be caused by wetlands or phreatophytes sustained, in part, by irrigation recharge. The missing groundwater / surface-water interactions should be verified to ensure this assumption is correct. The specific groundwater objects are: GW KRD South 2; GW KRD South 3; GW Sunnyside 6; and GW Westside 3.

• M&I Demands:

M&I demands in the model are assumed to be associated with landscape watering, and therefore use the irrigation demand pattern. There are no M&I demands during the non-irrigation season (November through February). A revised M&I pattern may need to be added to the model.

• Power Generation and Consumption:

While the model simulates flows through hydropower generation and pumping facilities, it does not calculate energy production or consumption. Power generation would need to be estimated outside of the YAKRW modeling effort.

2.3 Yakima River Basin Study - RiverWare Model Scenario Development

The preceding description of the YAKRW model is common to all versions of the model provided to HDR. To evaluate the effects of potential projects on water supplies and instream flows in the Yakima Basin, HDR needed to develop several versions of the model to represent conditions with and without the potential projects. For use in this study, HDR first developed a preliminary FWIP (Future without Integrated Plan) model using components of three RiverWare models provided by Reclamation. Next a Non-Storage Scenario was developed from the FWIP model. Finally the Integrated Plan scenario model was developed from the Non-Storage Scenario. Development of each scenario is described below and in Section 3.0.

Future without Integrated Plan Scenario

The No Action baseline model is referred to as the Future without Integrated Plan (FWIP) model. The component models were:

- 1. A current conditions model² reflecting current conditions from water years 1981 to 2005. This model was provided by the Reclamation Columbia Cascades Area Office (CCAO) and formed the basis of modeling used in the 2009 Department of Ecology Environmental Impact Statement.
- 2. A No Action model³ reflecting current conditions plus planned water conservation measures for water years 1981 to 2005. This model was also provided by Reclamation and formed the basis of modeling used in the 2008 Reclamation Environmental Impact Statement.
- 3. A revised current conditions model⁴ developed and provided by the TSC for use in climate change estimates.

² Model "2007.05.01_v4.8.3_Yakima_Basin_Network_25yr_Current"

³ Model "2007.05.01_v.4.8.3_Yakima_Basin_Network_25yr_NoAction"

⁴ Model "Yakima Planning Model"

Simulation object differences between the current conditions and revised current conditions, and the No Action versions of the Yakima model include:

- The proposed diversion to Wymer Reservoir occurs on the Yakima River from Taneum to Ellensburg reach (Thorp Diversion) in the No Action model and the Wilson to Umtanum reach in the current conditions model. Both models have Wymer releases to the Yakima River, Wilson to Umtanum reach.
- A pumped diversion occurs on the Yakima River in the Ahtanum to Parker reach to Union Gap Canal in the 2007 No Action model.
- Bumping reservoir in the 2007 No Action model is divided into three reservoirs; two of these represent extra water for fish and Roza purposes. The extra water from Bumping Reservoir bypasses the Parker gage for accounting purposes.
- Seepage from the KRD North Branch Canal immediately downstream of the bifurcation from the main canal returns to a location below Easton Reservoir in the 2007 No Action model. Seepage returns in the summer are 500 cubic feet per second (cfs), and there is no seepage in the winter months.

Based on the recommendation of the Reclamation CCAO-YFO operations personnel, the current conditions model revised by the CCAO-YFO for the RMJOC Modified Flows Study and by TSC for the RMJOC Climate Change Study was used as the initial basis for the FWIP model. The revised current conditions included but were not limited to:

- Ability to distribute shortages to nonproratable rights during more severe shortages
- Deliberate introduction of forecasting errors in estimating April TWSA
- Smoothing of changes to reservoir outflow targets to avoid unrealistically rapid release changes
- Bumping Reservoir minimum release targets adjusted based on available storage

The historic No Regulation No Irrigation inflows from the EIS current conditions model from November 1, 1980 to October 31, 2005 were transferred to the revised current conditions model to retain the same hydrology developed for the EIS. Planned water conservation measures in the previous Reclamation No Action model were also incorporated into the revised current conditions model. These are described in Section 3.1. Figure 11 illustrates the combination of models used to develop the FWIP model.

Non-Storage and Integrated Plan Scenarios

Once the HDR-modified FWIP model was finished, two additional models were developed using the FWIP model as the framework.⁵ HDR created a Non-Storage model that incorporated additional future enhanced water conservation measures and two groundwater storage and recovery locations (modeled at Thorp and at Marion Drain near Wapato Canal).

⁵ While referred to as separate models, from a model management perspective each "model" is a unique set of inputs to a single file. Using RiverWare rulebase programming, the model is reconfigured "on-the-fly" to generate a specific scenario. This allows noted errors and operational adjustments common to all scenarios to be applied or corrected in one file rather than maintaining separate model files. The inputs are described in detail in Section 2.5.

An Integrated Plan model was then created from the Non-Storage model by including several proposed storage projects and other potential structural changes in the Yakima Project. The three models and the assumptions used in each of them are discussed in greater detail in the sections below. Figure 12 illustrates the three HDR models.

2.4 Stakeholder Input

Model assumptions and operational changes were discussed with the CCAO operations personnel and Yakima River Basin fisheries experts from Reclamation and other agencies. Model results were provided to Reclamation after each change in modeling assumptions. Frequent emails and phone calls were exchanged to verify the suitability of modeled operations and assumptions.

Preliminary model results were presented at five Yakima River Basin Water Enhancement Project



FWIP (Study No Action Model) Figure 11. Model Components Used in Yakima Basin Study No Action Model

Workgroup meetings and four modeling subcommittee meetings from July to November of 2010. The workgroup consists of representatives from Reclamation, the Yakama Nation, Washington Department of Ecology, various irrigation districts, resource agencies, counties and municipalities in the basin, and environmental stakeholders. The modeling subcommittee group is a smaller, more focused team of individuals who are more familiar with the detailed operations of the Yakima River Basin and the RiverWare modeling efforts.

At each of the meetings, the preliminary results were presented and discussed, and suggestions were solicited for changes to be incorporated into the next round of model runs. Many of the changes to the FWIP and Non-Storage scenarios that resulted from stakeholder input were discussed above in Section 2.3.

Based on feedback from the CCAO, modeling subcommittee, and workgroup, the following changes were made, primarily to the Integrated Plan scenario model:

- 1. Revised Bumping Reservoir expanded storage to 190,000 acre-ft. Prior runs had been using a larger expanded storage option considered in Reclamation's storage study.
- 2. Bumping Reservoir minimum outflows revised based on operating rules provided by Anchor/QEA.
- 3. Irrigation conservation benefits first apply to achieving a full irrigation supply and then to increasing storage in reservoirs. Some irrigation districts were previously assumed to always provide irrigation conservation to decrease reservoir releases.

- 4. Revised water conservation values to reflect conservation already achieved and what will be achieved both with and without the additional funding associated with the Integrated Plan.
- 5. Adjusted spring pulse flows on a year-by-year basis. Reservoirs will not release a spring pulse flow if it occurs naturally.
- Used a revised storage carryover target table provided by Reclamation that includes an expanded Bumping Reservoir storage.



Figure 12. Relationship of Project RiverWare Models

- 7. Parker Title XII flows are calculated based on original reservoir storage plus storage in groundwater recharge projects, Wymer instream flow storage water account, and instream conservation benefits. Previously all proposed and existing project storage was applied, which further increases Title XII flows. Title XII flows refer to the target flows that have been defined at two points in the Yakima River Basin, as mandated by Congress through the Yakima River Basin Water Enhancement Project (Title XII of the Act of October 31, 1994, United States Congress [Public Law 103-434]). Target flows are defined in a manner that allows them to be increased as more conservation elements of YRBWEP are implemented over time.
- 8. Two prorationing values are calculated. The first is based on the original system and applied to Sunnyside and Tieton demands. The second is based on the Integrated Plan and applies to all other (non-Sunnyside and non-Tieton) prorated demands.
- 9. Returned the flip-flop and mini-flip-flop functions for the FWIP and Non-Storage scenarios to their original configuration. Flip-flop operations are only adjusted under the Integrated Plan scenario.
- 10. Increased Kachess inactive storage tunnel/pump capacity from 1,000 cfs to 1,200 cfs, based on current engineering analysis. This capacity can limit the model's ability to completely use Kachess inactive storage during a single year.
- 11. Wymer Reservoir can fill from Cle Elum releases (which are diverted to the instream storage account) and from flood flows above 1,000 cfs (which are diverted to the irrigation storage account).
- 12. Irrigation storage for proposed projects is utilized only when prorationing without the projects is below 70 percent. Only a portion of this storage is used to increase prorationing to 70 percent, reserving remaining storage for future dry years.
- 13. Revised proposed groundwater recharge areas are based on preliminary hydrogeologic parameters provided by Golder Associates (see Groundwater Infiltration Report).

- 14. The modeling function "Forecast System September 1 Storage" was changed to always use the storage in each reservoir. This previously was linked to a function that included expanded storage only if proration was less than or equal to 70 percent. This was usually causing forecasting of the September 1 carry-over storage to be too low. It is not clear how the groundwater recharge storage should be included in this forecast.
- 15. Modified the slot "TWSA PARW_Data. MaximumCarryoverStorage". This was previously hard-coded to 1,066,000 acre-feet, which limits the September 1 forecast carryover storage. This slot was replaced with an expression slot that increased the maximum carryover storage if expanded storage options are used.
- 16. Added new flip-flop factors in tables "MiddleYakimaSystemStatus, FlipFlop Table" and "NachesSystemStatus. Rimrock Bumping Release Table". The "Proration" column is used if proration levels are less than or at 70 percent. The intent is to move demand from the upper Yakima to the Naches system sooner and split demand between Bumping and Rimrock. This is to address the comment that 1993 releases from Rimrock were too low and Kachess outflows were too high. This draws down Bumping and Rimrock more than previously, although the Kachess full dead pool is only partially used.
- 17. Added a 1 percent proration buffer to the function "Use Integrated Plan Projects". This function triggers calling for additional storage if proration is less than or at 70 percent. The function may not have the desired effect if proration is slightly above 70 percent prior to the proration date since the Water Supply Available for Irrigation calculation is fixed to values occurring at the proration date. As a result, 1 percent was added (71 percent proration trigger) before the proration date to attempt to avoid this condition.

2.5 Revisions to Model Operation

HDR revisions to the Reclamation model primarily involved additional datasets. These datasets, combined with revised rules, determined if the model operated in FWIP, Non-Storage, or full Integrated Plan scenarios. The following datasets were added to the model:

- Historic Inflows: The Not Regulated Not Irrigated hydrology was transferred to a separate dataset. For model runs that did not involve climate change scenarios, a model operating rule would copy this dataset to the inflow inputs of reservoirs and river reaches.
- VIC (Variable Infiltration Capacity) Inflows: This dataset contained the hydrology generated from the global climate change models. Based on a specific climate change scenario, the appropriate hydrology is copied to inflow inputs of reservoirs and river reaches.
- System Diversions: In the original Reclamation model, each canal with water conservation measures had a specific rule with hard-coded conservation parameters. In the full Integrated Plan, the number of conservation measures had increased. Different scenarios also applied to different conservation approaches. The System Diversions dataset was created to have a uniform approach to estimating conservation benefits for any number of canal systems. Rules were made generic by looping through each canal and extracting values from this dataset.
- Integrated Plan Projects: The Integrated Plan Projects is the primary table used to configure the model among different scenarios. Based on inputs in this table, the model will operate in the FWIP, Non-Storage, or Integrated Plan scenario.

Table 6 shows the settings that are available within the Integrated Plan projects model data object:

		MODEL SETTINGS FOR:			
PARAMETER AND DESCRIPTION	FWIP	NON-STORAGE	INTEGRATED PLAN		
Conservation. Active					
Determines if a conservation line item is enabled	Varias by assal lasstica				
0=Conservation line item not used		valles by calla	TIOCALION		
1=Conservation line item is used					
Conservation. Total Conservation	Varias by canal location				
The total conservation savings in acre-feet per year during full water supply	varies by canal location				
Conservation. Instream Conservation					
The portion of the conservation savings, in acre-feet per year, applied to instream	Varies by canal location				
flow benefits	-				
Conservation. Irrigation Conservation					
The portion of conservation savings, in acre-feet per year, applied to irrigation		Varies by cana	I location		
benefits		T			
Conservation. Full Irrigation Supply					
A setting determining if the irrigation benefit will first go to achieving a full irrigation			1		
supply during water short years	1	1			
0=Irrigation benefit will always reduce diversions and reservoir releases					
1=Irrigation benefit will first increase deliveries to achieve a full irrigation supply					
and then to reducing diversions					
Point of Diversion Changes. Active		Varies by cana	Llocation		
Determines if a point of diversion change line item is active. If active, the existing	Benton and Wapato changes are included in all				
diversion is removed and the proposed river diversion is used	scenario	s. Naches Selah po	int of diversion change		
0=Proposed point of diversion change is not active	ooonane	is included in the Int	tegrated Plan.		
1=Proposed point of diversion change is active					
Proposed Wymer Reservoir. Active		0			
A value of 0 configures the model to not use the proposed Wymer Reservoir while	0	0	1		
a value of 1 activates the reservoir.					
Proposed Wymer Reservoir. In Stream Account			00 500		
The portion of the proposed Wymer Reservoir, in acre-feet, allocated for supply of	n/a	n/a	82,500		
Instream flows					
Proposed Wymer Reservoir. Irrigation Account	nlo	nla	00.000		
The portion of the proposed wymer Reservoir, in acte-reet, allocated for supply to	n/a	n/a	ăU,UUU		
Roza Imgalion District					
The capacity of the Thern pipeline which delivers inflows to Wymer Deservoir	n/a	n/a	1,000 cfs		
The capacity of the Tholp pipeline which delivers inhows to wymer Reservoir					
Ploposed Wylfiel Reservoll. Will Flow The minimum flow in the Vakima Diver helew which Thern nineline will not divert			1,000 cfs		
uprogulated water. Clo Elum and Koechelus recerveir releases specifically for	n/a	nla			
supply to Wymor ride on ton of the unregulated water and always diverted at	11/4	11/a			
Thorp					
Pronosed Wymer Reservoir, Skim Fraction					
The nortion of the excess unregulated Vakima River water above the minimum	n/a	n/a	0.90		
flow which is diverted into the Thorn nineline	n/a	n/a	0.70		
Proposed Wymer Reservoir, Storage Supplemental					
Configures whether Cle Elum and Keechelus reservoirs can release storage to					
supply to Wymer. A value of 0 indicates that only unregulated flows can be					
diverted into Wymer. Diverted flows are allocated equally to instream and irrigation	n/a	n/a	1		
Wymer storage accounts. A value of 1 indicates that upper reservoir storage can					
be released to Wymer. Water from reservoir releases are accrued to the instream					
flow account while unregulated water diversion accrued to the irrigation account.					
Groundwater Recharge New Areas. Active					
Indicates if the aquifer recharge and recovery projects are active. A value of 0			1		
indicates that the project is not used, while a value of 1 allows the proposed project	0	· · · ·	1		
to be used					
Groundwater Recharge New Areas. Min Flow					
The minimum flow in the Yakima River below which the recharge project will not	n/a	1,000 cfs	1,000 cfs		
divert water					

Table 6. Integrated Plan Projects Model Settings

		MODEL SETTINGS FOR:		
PARAMETER AND DESCRIPTION		NON- STORAGE	INTEGRATED PLAN	
Groundwater Recharge New Areas. Skim Fraction The portion of Yakima River flows, above the minimum flow amount, which can be diverted into the recharge area basin	n/a	0.90	0.90	
Groundwater Recharge New Areas. Max Flow The maximum monthly infiltration rate which can be diverted into the recharge project basin.	n/a	300 cfs	300 cfs	
Groundwater Recharge New Areas. Max Annual Volume The maximum annual diversion allowed into the recharge project.	n/a	54,000 acre- feet	54,000 af	
Groundwater Recharge New Areas. Alpha Coefficient The rate at which recharged water passively returns to the Yakima River as baseflow, specified in units of 1/day.	n/a	0.0070	0.0070	
Groundwater Recharge New Areas. Portion Pumped The portion of recharged water which is actively recaptured through wells for direct irrigation application	n/a	0	0	
Proposed K to K Pipeline. Active Determines if the proposed pipeline between Keechelus and Kachess reservoirs is active. A value of 0 is inactive while 1 allows flow through the pipeline	0	0	1	
Proposed K to K Pipeline. Pipeline Capacity The physical capacity of the pipeline.	n/a	n/a	400 cfs	
Proposed K to K Pipeline. Pipeline Invert The elevation of the pipeline invert in Keechelus reservoir; flow is not physically permitted to occur below this elevation	n/a	n/a	2425.00 ft	
Proposed K to K Pipeline. Keechelus Target Storage The minimum target storage in Keechelus. Flow is not permitted in the pipeline when Keechelus is below this storage amount. Roughly set to prevent complete drawn down of Keechelus in the worse year that is simulated.	n/a	n/a	60,000 af	
Proposed K to K Pipeline. Kachess Target Storage The maximum storage in Kachess during the flood control season, above which pipeline flow is not permitted. Roughly set to prevent additional flood control spills from occurring. Outside of the flood control season Kachess target storage is the top of the conservation pool	n/a	n/a	450,000 af (including the dead pool volume)	
Proposed K to K Pipeline. Smolt Restriction Restriction on the pipeline capacity for smolt migration from March 31 st to August 1 st	n/a	n/a	200 cfs	
Proposed Kachess Inactive Storage. Active Indicates if use of the dead pool storage in Kachess can be used to meet water supply and instream flow targets. A value of 0 limits reservoir withdrawals to the top of the dead pool while a value of 1 permits dead pool draw drawn during water short years	0	0	1	
Proposed Kachess Inactive Storage. Percent Usable In Active Storage HDR estimated storage of 250,000 acre-feet below the top of the dead pool. This fraction limits the extent of dead pool drawn down, determined as 200,000 acre-feet (or 81% of 250,000 acre-feet) by the modeling subcommittee	n/a	n/a	0.81	
Proposed Kachess Inactive Storage. Pump Capacity The tunnel or pumping capacity used to access flows from the dead pool.	n/a	n/a	1,200 cfs	
Proposed Cle Elum Raise. Active Determines if Cle Elum reservoir dam is raised an additional 3 feet. A value of 0 uses the existing dam height while a value of 1 runs the model with expanded storage.	0	0	1	
Proposed Bumping Reservoir. Active Determines if Bumping Reservoir is expanded. A value of 0 uses the existing Bumping storage while a value of 1 models an expanded storage	0	0	1	
Proposed Bumping Reservoir. Max Storage The size of the expanded Bumping reservoir; the model allocates the same flood space size as in the existing reservoir	n/a	n/a	190,000 af	

		MODEL SETTINGS FOR:		
PARAMETER AND DESCRIPTION	FWIP	NON- STORAGE	INTEGRATED PLAN	
Proposed Instream Flows. Active Determines if additional stream flows considered by the instream flow subcommittee are modeled. A value of 0 defaults the model to the existing instream flow target, while a value of 1 uses the instream flow subcommittee values	0	0	1	
Keechelus Max Outflow. Max Outflow Places limitations on the maximum outflow of Keechelus below the physical release restrictions. For the integrated plan, this table augments mini-flip-flop and K to K pipeline operations by reducing flows from July to the end of the irrigation season	4,000 cfs	4,000 cfs	120 to 4,000 cfs	
Projects Proration Trigger Proration trigger below which proposed integrated plan projects (Wymer irrigation account use, Kachess inactive storage, Cle Elum and Bumping expanded storage) are used	n/a	n/a	0.70	
Use Conservation Seepage Rates Specifies if the existing condition canal seepage rates (value of 0) or reduced conservation seepage rates (value of 1) are used	0	1	1	
No Carryover During Proration Determines if the 85,000 acre-feet system carryover storage is suspended to maximize use of storage when the proration trigger is active	0	0	1	
Use Future M&I Specifies if M&I demands are increased to a year 2040 conditions. A value of 1 permits the increase while a value of 0 uses existing condition demands	1	1	1	
Hydrologic Dataset Specifies the hydrologic inflow dataset that is used. Values are: 0 = historic NRNI 1 = replication of historic conditions from global climate change model 2 = cgcm31t47 climate change scenario 3 =hadcm climate change scenario 4 =hadgem1 climate change scenario	0	0	0 to 4	

Table 6. Integrated Plan Projects Model Settings (cont.)

3.0 Modeled Scenarios under Existing Hydrology

This section summarizes the primary elements of each modeled scenario under existing hydrologic conditions (without future climate change). The final subsection presents the simulation results from the final simulation runs for each scenario. The scenarios include Future without Integrated Plan (FWIP), Non-Storage, Integrated Plan, and Adjusted Integrated Plan.

3.1 Future without Integrated Plan Scenario

The FWIP model was developed to represent the No Action scenario. This model incorporates conservation projects that have been completed or are in the process of being completed under the Yakima River Basin Water Enhancement Project. It also incorporates expected growth in municipal uses and domestic wells that may require water deliveries for supply or mitigation.

Conservation

Conservation measures modeled in the FWIP scenario include projects by the Roza, Sunnyside and Benton irrigation districts. Conservation water savings can be applied to a combination of irrigation or instream needs. Irrigation conservation benefits serve to either increase delivered water supply during water-short years or reduce reservoir releases in full supply years. Instream conservation benefits increase the instream flow target at Parker gage. Benefits to irrigation are applied as conservation occurs.
As irrigation deliveries peak in the summer, the irrigation conservation benefits also peak. Benefits for instream flows are applied based on paper accounting⁶. The total conservation benefit for the year is forecasted at the beginning of the irrigation season. The instream flow conservation benefit is applied uniformly throughout the irrigation season. This results in debits from irrigation to instream purposes at the beginning of the season, which are paid back later in the season.

Conservation by the Roza Irrigation District is solely for irrigation benefit, whereas conservation at Sunnyside and Benton irrigation districts applies to both instream and irrigation benefits. These conservation measures have been advanced by the modeling subcommittee group as having either already occurred (but not reflected in model demand inputs) or will occur in the future with secured funds (see Table 7).

		U	1 <i>1</i>
LOCATION	TOTAL CONSERVATION (ACRE-FEET/YEAR)	INSTREAM BENEFIT (ACRE-FEET/YEAR)	IRRIGATION BENEFIT (ACRE-FEET/YEAR)
1: RZCW Roza	36,000	0	36,000
3: SNCW Sunnyside	54,600	36,400	18,200
4: BENW Benton	6,870	5,420	1,450

Table 7. Conservation In Future Without Integrated Plan (FWIP)

Notes: Conservation amounts are based on a full water supply. Proration will result in lower realized conservation. Irrigation benefit may accrue through decreased reservoir releases during a full water supply or increased diversions during prorated years to obtain a full irrigation supply.

Point of Diversion Changes

The intended benefit of point of diversion (POD) changes is to move the diversions closer to the point of use to leave the water in the river longer and maintain higher river flows in targeted reaches. Two POD changes were modeled under the FWIP scenario; the Benton Irrigation District (BID) project and the WIP 50 cfs project. The BID POD was relocated from the Sunnyside canal diversion to a new diversion on the Yakima River about 70 miles downstream at Benton City. To simulate the change, Sunnyside canal diversions were reduced by the ratio of Benton Irrigation District volume to total Sunnyside volume (18,520 acre-feet to 458,520 acre-feet), or approximately 4 percent.

The second POD change involved using Satus Creek pumps to move approximately 50 cfs of diversion from the Wapato main canal to a location downstream of Granger. The pumps are used when diversions into the canal exceed 50 cfs. This typically allowed the pumps to operate from March 17 to October 18.

Future Municipal and Industrial Consumptive Demands

Future M&I for 2040 is applied to the upper Yakima River (Kittitas County area estimate), Yakima River below the Naches (Yakima County area estimate), and lower Yakima River (Benton County area estimate). The annual values and monthly use pattern were obtained from the draft out-of-stream water needs report prepared for the Yakima Basin Study⁷. The annual consumptive amounts are distributed from April to October, based on an average M&I pattern above the winter uses. The amounts are (in acre-feet per year): 9,100 for Yakima Co.; 1,600 for Kittitas Co. and 1,100 for Benton. The M&I pattern was selected to reflect the consumptive use portion of the demand, not non-consumptive return flows. As described in the out-of-stream report, future M&I demands include population growth, conservation, and the net water increase after converting agricultural water rights to M&I use within the Urban

⁶ Paper accounting means that the quantity of water was tabulated from water right or other legal document stating how much water should or is being used. The paper amount is not an indicator of actual water in the river. For example, you can have more paper water (i.e. water allocated thru water rights) than water actually flowing in the river.

⁷ HDR Engineering and Anchor QEA, "Yakima River Basin Study: Water Needs for Out-of-Stream Uses", Draft, August 2010.

Growth Boundary (see M&I Demands TM). This includes potential mitigation needs associated with domestic wells. It is possible that future M&I demands might be constrained by the available water rights. For this analysis the assumption was that future demand would not be water-right limited.

3.2 Non-Storage Scenario

The Non-Storage model was developed to include additional conservation measures, POD changes, and two groundwater storage and recovery projects. These features are also included in the Integrated Plan model.

Conservation

The Non-Storage scenario included modeling of additional conservation measures and the three conservation projects from the FWIP model. Each of the new conservation projects provide irrigation benefits only. No Wapato conservation projects were considered, based on the assumption that conserved water from these projects would contribute to full build-out of tribal irrigation. Table 8 summarizes conservation projects in the Non-Storage and Integrated Plan scenarios.

LOCATION	TOTAL CONSERVATION (ACRE-FEET/YEAR)	INSTREAM BENEFIT (ACRE-FEET/YEAR)	IRRIGATION BENEFIT (ACRE-FEET/YEAR)
0: KTCW Kittitas	40,735	0	40,735
1: RZCW Roza	36,000	0	36,000
2: RZCW Roza	23,900	0	23,900
3: SNCW Sunnyside	54,600	36,400	18,180
4: BENW Benton	6,870	5,420	1,450
5: KTCW Kittitas	2,000	0	2,000
6: WESW Westside	600	0	600
7: WESW Westside	2,618	0	2,618
8: ELTW Ellensburg Town	3,026	0	3,026
9: CADW Cascade Pumps below Slide	2,088	0	2,088
10: CADW Cascade Pumps below Slide	2,579	0	2,579
11: BUCW Bull	639	0	639
12: BUCW Bull	429	0	429
13: UNGW Union Gap	200	0	200
14-16: Wapato	0	0	0
17: SNCW Sunnyside	4,265	0	4,265
18: SOUW South Naches	9,733	0	9,733
19: NSCW Naches Selah	16,675	0	16,675
20: KNCW Kennewick	28,200	0	28,200

Table 8. Conservation in Non-Storage and Integrated Plan Scenarios

Notes: Conservation amounts are based on a full water supply. Proration will result in lower realized conservation in years with supply shortages. Irrigation benefit may accrue through decreased reservoir releases during a full water supply, or increased diversions during prorated years to move water users closer to a full irrigation supply.

Canal seepage rates are reduced to reflect conservation from canal lining. When seepage is reduced, the amount of water delivered to the canal turnout is kept constant (except in times of shortage), but the amount of water that must be diverted from the river is reduced. Table 9 shows the revised seepage rates provided by Anchor QEA. Conservation was not differentiated between canal and on-farm improvements. Conservation benefits were modeled as a reduction in reservoir releases during times of full supply or as an improvement in shortage deliveries. Return flows were reduced based on an assumption by Anchor QEA regarding the proportion of the benefits derived from canal lining.

	CANAL SEEPAGE RATES				
CANAL	NON-CONSERVATION	FULL CONSERVATION			
	CONDITION	CONDITION			
KRD	48%	48%			
Roza	36%	36%			
Sunnyside	36%	36%			
Cascade	36%	25%			
Town	36%	25%			
Westside	36%	25%			
Wapato	36%	32%			
Bull	36%	25%			
Other Irrigation Canals	36%	36%			
M&I systems	50%	50%			

Table 9. Canal Seepage Rates

Point of Diversion Changes

The Benton Irrigation District and Satus Creek pump diversion changes in the FWIP were retained under this Non-Storage scenario. The Kennewick POD was changed to the Columbia River and no Kennewick water is diverted from the Yakima basin.

Future M&I Consumptive Demands

The same future M&I consumptive demands from FWIP were modeled in the Non-Storage scenario.

Groundwater Storage and Recovery

Two groundwater storage and recovery locations were modeled one at Thorp and another at Marion Drain (near Wapato Canal). Diversions during the non-irrigation season (November through February) were made if river flows were above 1,000 cfs. No more than 90 percent of the flow above 1,000 cfs was diverted up to a maximum rate of 10,000 acre-feet per month or 50,000 acre-feet per year for each project. Groundwater recovery occurs passively (increased base flow over time to Yakima River) at a rate of 0.01/day (that is, 1 percent of the volume in aquifer storage is released each day) at Thorp and 0.005/day (one-half of 1 percent is released each day) at Marion Drain. These release rates correspond to approximately a 70-day and a 140-day average return period, respectively. No active recovery (pumping out of the aquifer based on irrigation needs) is modeled. Estimates of monthly and annual infiltration rates and return rates were provided by Golder (see Groundwater Infiltration Report).

3.3 Integrated Plan Scenario

In addition to the Non-Storage elements, the Integrated Plan includes a new reservoir at Wymer, a pipeline from Keechelus to Kachess, access to Kachess inactive storage, a 3 foot raise of the Cle Elum Dam, an enlarged Bumping Reservoir, and enhanced stream flows.

Conservation

Conservation projects listed in the Non-Storage scenario were used in modeling the Integrated Plan scenario.

Point of Diversion Changes

Point of diversion changes listed in the Non-Storage scenario were used in the Integrated Plan scenario. Additionally, the diversion for Naches Selah irrigation is moved to the Wapatox Canal.

Future Municipal and Industrial Consumptive Demands

The same M&I future consumptive demands from the FWIP are used.

Groundwater Storage and Recovery

Groundwater storage and recovery projects listed in the Non-Storage scenario were used in the Integrated Plan scenario.

Proposed Wymer Reservoir

The capacity of the proposed Wymer Reservoir is 162,500 acre-feet. The reservoir was split into two storage accounts – 82,500 acre-feet to provide benefit to instream flow and the remaining 80,000 acre-feet to provide additional irrigation supply. The proposed reservoir is filled by diverting water from the Yakima River at Thorp during winter and spring, keeping a minimum of 1,000 cfs in the river. The Thorp pumping and pipeline capacity is 1,000 cfs. During the non-irrigation season, flood flows exceeding 1,000 cfs (and exceeding diversion to groundwater recharge) can be diverted into the irrigation storage account of Wymer. Lake Cle Elum can release flows up until the storage control date for accrual in the instream storage account in Wymer. The irrigation storage account contributes to total water supply available only at times when prorationing without Integrated Plan projects is less than 70 percent. Wymer irrigation water can only be used to the extent needed to bring prorationing up to 70 percent. The instream account does contribute to total water supply available each year and is applied to Parker gage minimum flows between July and the end of September.

Proposed Keechelus to Kachess Pipeline

The 5-mile-long pipeline from Keechelus Lake to Kachess Lake is intended to reduce high flows during the summer time caused by reservoir releases in the river below Keechelus and capture additional storage that may be spilled. Pipeline capacity of 400 cfs, is reduced to 200 cfs after March 31 based on the smolt migration, then increased to 400 cfs after August 1st. Transfers would occur when Keechelus is above 60,000 acre-feet and would stop if Keechelus drops below this level (this level was arbitrarily set to maintain some storage in Keechelus during the worst drought year). Flows into Kachess occur if Kachess is below 450,000 acre-feet (includes 248,000 acre-feet of inactive storage of which 48,000 acre-feet is inaccessible) during the flood season (to prevent additional spills from Kachess) or below the conservation pool in non-flood season.

Kachess Inactive Storage

Revisions were made to the outlet works (using a tunnel or a pump station) to allow the reservoir to be drawn down by an additional 200,000 acre-feet when prorationing is less than 70 percent. The maximum outlet capacity is modeled at 1,200 cfs. While prorationing will be recalculated when inactive storage is used, Title XII flows will not consider additional storage in the inactive pool. The outlet from the inactive storage is currently assumed to go to Lake Easton.

Proposed Cle Elum Dam Raise

A 3-foot increase of the maximum flood pool and conservation pool was modeled in the Integrated Plan. Total water supply available and prorationing consider this expanded pool when prorationing falls below 70 percent. No other operational changes were made to Cle Elum. Title XII flows will not consider the expanded pool storage.

Proposed Bumping Reservoir Expansion

Bumping Reservoir was increased to 190,000 acre-feet total size, which may be limited to approximately 156,000 acre-feet during the flood-control season based on existing guidance and

operations practices. The current size of the flood pool is maintained, with elevations increased. Prorationing will consider the expanded Bumping Reservoir storage when prorationing falls below 70 percent. Title XII flows will not consider expanded Bumping Reservoir storage. Bumping may release flows to cover irrigation shortages on the Naches when Rimrock Reservoir is depleted. No other operational changes are made. For example, the Bumping Reservoir is not divided into irrigation and instream accounts. The initial (starting) storage for the expanded Bumping Reservoir is set at 100,000 acre-feet.

Enhanced Instream Flow Operations

Enhanced instream flows were incorporated by modifying minimum flows in the Keechelus, Cle Elum, Easton, lower Naches and Tieton reaches. The Keechelus minimum flow is set at 120 cfs, with a 7-day spring flood pulse near the end of April, peaking at 500 cfs. The date of the spring flood may change each year to make use of the natural hydrograph, and the peak is not supplemented by reservoir releases if it already reaches 500 cfs. The Cle Elum minimum flow is 300 cfs, with a spring flood pulse of 1,000 cfs. This peak is also not supplemented if reached naturally. The Easton reach uses a 250-cfs minimum flow, decreasing to 220 cfs from September to December. The spring pulse flow is 1,000 cfs at this location. The Tieton reach has a minimum flow of 125 cfs from October to April, while the lower Naches reach minimum flow is 550 cfs between June and October.

Minimum outflows from Bumping Reservoir vary based on the storage in the reservoir. During winter, the minimum flow depends on storage and minimum target outflow of 130 cfs. Between April 15 and April 29, the flow increases to 365 cfs, when storage is less than 75,000 acre-feet, to 500 cfs for higher storage. Between April 29 and May 20, the flow increases further, to between 600 and 900 cfs. The minimum flow rate declines to between 365 cfs and 500 cfs until September 1, followed by a return to the winter flow rate. If the projected April 1 TWSA is less than 2.4 million acre-feet (MAF), the maximum minimum flow released is 600 cfs.

Outflows from Keechelus Lake are limited to no more than 500 cfs in July, decreasing to 120 cfs from the end of August to the end of the irrigation season. Water demands that cannot be met from Keechelus Lake as a result of these maximum flow levels are transferred to other reservoir releases.

3.4 Adjusted Integrated Plan Scenarios

The Integrated Plan scenario described above was modified to produce three different adjusted scenarios representing water supply and instream flow conditions with a part of the Integrated Plan eliminated. The three adjusted scenarios are:

- 1. Integrated Plan without Kachess Inactive and without Keechelus to Kachess Pipeline
- 2. Integrated Plan without Bumping Reservoir enlargement
- 3. Integrated Plan without Wymer Reservoir.

Detailed refinement of modeling assumptions and operational rules was not conducted in developing and simulating these adjusted scenarios. Instead the relevant portions of the Integrated Plan scenario model were simply switched off.

3.5 Model Scenario Results

Results for the FWIP, Non-Storage, Integrated Plan, and Adjusted Integrated Plan scenarios are summarized below and in the figures and tables in Appendix B and C. The hydrologic data under which the scenarios were modeled represent conditions that occurred historically from 1981 through 2005. This historic period was chosen to test future operations and facilities because it had the most complete data

available on conditions in the basin. The period included multiple dry years and one period (1992-1994) of three consecutive dry years.

FWIP Results

The Future without the Integrated Plan scenario provides a baseline condition against which the effects of the planned projects can be compared. Table 10 summarizes the water resources conditions under FWIP. The critical conclusions related to water supply are as follows:

- Average April total water supply available is 2.79 MAF
- Average April to September diversion is 1.61 MAF
- Average September 30 reservoir storage totals 0.23 MAF
- Average prorationing level is 80 percent

For the four dry years summarized:

- Minimum April total water supply available is 1.71 MAF
- Minimum April to September diversion is 1.23 MAF
- Minimum September 30 reservoir storage totals 0.04 MAF
- Minimum prorationing level is 21 percent; Average prorationing level is 31 percent

Simulated instream flow conditions for FWIP are summarized in the Instream Flow Technical Memorandum. The results show that there are significant deficiencies in the instream flows under FWIP conditions.

Resource indicator (measurement)	Future without Integrated Plan	Integrated Plan	Change from FWIP				
Average for water years 1981–2005 (maf)							
April 1 total water supply available (TWSA)	2.79	3.00	0.22				
April–September Parker flow volume	0.64	0.60	-0.04				
April–September diversion	1.61	1.69	0.09				
September 30 reservoir contents	0.23	0.58	0.34				
Irrigation proration level	80%	92%	12%				
<u> 1993 dry-year (</u>	maf)	-	-				
April 1 total water supply available (TWSA)	2.06	2.24	0.18				
April–September Parker flow volume	0.36	0.30	-0.06				
April–September diversion	1.42	1.57	0.15				
September 30 reservoir contents	0.04	0.26	0.21				
Irrigation proration level	44%	70%	26%				
<u>1994 dry-year (</u>	maf)						
April 1 total water supply available (TWSA)	1.74	2.22	0.48				
April–September Parker flow volume	0.31	0.25	-0.07				
April–September diversion	1.23	1.52	0.29				
September 30 reservoir contents	0.05	-0.07	-0.11				
Irrigation proration level	21%	70%	49%				
2001 dry-year (maf)						
April 1 total water supply available (TWSA)	1.76	2.45	0.69				
April–September Parker flow volume	0.25	0.20	-0.05				
April–September diversion	1.29	1.55	0.27				
September 30 reservoir contents	0.06	0.22	0.16				
Irrigation proration level	32%	70%	38%				
2005 dry-year (maf)							
April 1 total water supply available (TWSA)	1.71	2.32	0.61				
April–September Parker flow volume	0.25	0.18	-0.06				
April–September diversion	1.25	1.53	0.28				
September 30 reservoir contents	0.08	0.12	0.05				
Irrigation proration level	28%	70%	42%				
Shading above greater than 10% improvement from EV		Prorotioning	> 70%				

Table 10. FWIP and Integrated Plan Water Resources Modeling Results

Shading shows greater than 10% improvement from FWIP conditions, or Prorationing >70%. Shading shows greater than 10% decrease from FWIP conditions, or Prorationing <70%.

* September 30 reservoir contents do not include 200,000 acre-feet of inactive storage in Kachess that is available in critically dry years under scenarios that include that project.

Non-Storage Results

The Non-Storage scenario provides an interim condition against which the effects of the major reservoir storage projects can be compared. Table 11 summarizes the water resources conditions under the Non-Storage scenario. The critical conclusions related to water supply are as follows:

- Average total water supply available is 2.87 MAF
- Average April to September diversion is 1.58 MAF
- Average September 30 reservoir storage totals 0.27 MAF
- Average prorationing level is 81 percent

For the four dry years summarized:

- Minimum total water supply available is 1.79 MAF
- Minimum April to September diversion is 1.23 MAF
- Minimum September 30 reservoir storage totals 0.04 MAF
- Minimum prorationing level is 22 percent

Simulated instream flow conditions for the Non-Storage scenario are essentially unchanged from baseline or FWIP conditions, since reservoir operations are not changed in the scenario. The results show that there are significant deficiencies in the instream flows under Non-Storage scenario conditions.

Integrated Plan Results

The Integrated Plan scenario results represent the conditions and the benefits associated with the project. The water resources conditions under the Integrated Plan scenario (and the change from the FWIP scenario conditions) are summarized in Table 10. The critical conclusions related to water supply are as follows:

- Average total water supply available is 3.00 MAF
- Average April to September is 1.69 MAF
- Average September 30 reservoir storage totals 0.58 MAF
- Average prorationing level is 92 percent

For the four dry years summarized:

- Minimum total water supply available is 2.22 MAF
- Minimum April to September diversion is 1.52 MAF
- Minimum September 30 reservoir storage totals 0.13 MAF (including 0.20 MAF in Kachess Inactive)
- Minimum prorationing level is 70 percent

The Integrated Plan scenario includes reservoir releases to meet reach-specific target flows. The relative success of achieving the simulated targets are summarized in the Instream Flow Technical Memorandum and in Figure 13 below. Hydrographs displaying the reach-by-reach flow improvements are included in Appendix B. The results show that the Integrated Plan would help meet flow objectives in 13 of 14 critical reaches, including substantial improvement in six reaches. In addition, nearly 200,000 acre-feet of additional water left in September 30 carryover storage could be used to provide additional improvement in flows in certain critical years, if desired. It should be noted that after the inactive storage is used, it would have to be refilled before being used again, and likely would not be available in consecutive years. Also, power subordination at Chandler and construction of the KRD South Branch project (which are not included in the modeling results) could also significantly improve flows on the lower Yakima and in many flow-deficient tributaries for the Integrated Plan.

Table 11. FWIP and Non-Storage Scenario Water Resources Modeling Results					
Resource indicator (measurement)	Future without Integrated Plan	Non- Storage	Change from FWIP		
WATER RESOU	RCES				
Average for water years 1	<u>981–2005 (maf)</u>				
April 1 total water supply available (TWSA)	2.79	2.87	0.08		
April–September Parker flow volume	0.64	0.68	0.04		
April–September diversion	1.61	1.58	-0.03		
September 30 reservoir contents	0.23	0.27	0.04		
Irrigation proration level	80%	81%	1%		
<u>1993 dry-year (</u>	maf <u>)</u>		-		
April 1 total water supply available (TWSA)	2.06	2.11	0.05		
April–September Parker flow volume	0.36	0.36	0.00		
April–September diversion	1.42	1.42	0.00		
September 30 reservoir contents	0.04	0.04	0.00		
Irrigation proration level	44%	47%	2%		
<u>1994 dry-year (</u>	maf)	_	_		
April 1 total water supply available (TWSA)	1.74	1.79	0.05		
April–September Parker flow volume	0.31	0.31	0.00		
April–September diversion	1.23	1.23	0.00		
September 30 reservoir contents	0.05	0.04	0.00		
Irrigation proration level	21%	22%	2%		
2001 dry-year (maf)	_	_		
April 1 total water supply available (TWSA)	1.76	1.86	0.10		
April–September Parker flow volume	0.25	0.25	0.00		
April–September diversion	1.29	1.32	0.04		
September 30 reservoir contents	0.06	0.05	0.00		
Irrigation proration level	32%	37%	5%		
2005 dry-year (maf)					
April 1 total water supply available (TWSA)	1.71	1.80	0.09		
April–September Parker flow volume	0.25	0.25	0.01		
April–September diversion	1.25	1.28	0.03		
September 30 reservoir contents	0.08	0.07	0.00		
Irrigation proration level	28%	33%	4%		

Shading shows greater than 10% improvement from FWIP conditions, or Prorationing >70%.

Shading shows greater than 10% decrease from FWIP conditions, or Prorationing <70%.



Figure 13. Improvements in Instream Flows

Adjusted Integrated Plan Results

The Integrated Plan scenario described above was modified to produce three different adjusted scenarios representing water supply and instream flow conditions with part of the Integrated Plan eliminated. The results from the three Adjusted Integrated Plan scenarios are summarized in Table 12.

			IP w/o	IP w/o					
Resource indicator	Future without	Integrated	Bumping	Kachess	IP w/o				
(measurement)	Integrated Plan	Plan	Enlarge.	& KtoK	Wymer				
	WATER RESOUR	RCES							
<u>Average f</u>	<u>Average for water years 1981–2005 (maf)</u>								
April 1 total water supply available (TWSA)	2.79	3.00	2.96	3.00	2.88				
April–September Parker flow volume	0.64	0.60	0.60	0.61	0.65				
April–September diversion	1.61	1.69	1.69	1.69	1.59				
September 30 reservoir contents	0.23	0.58	0.43	0.59	0.35				
Irrigation proration level	80%	92%	91%	91%	85%				
	<u>1993 dry-year (r</u>	<u>naf)</u>							
April 1 total water supply available (TWSA)	2.06	2.24	2.19	2.26	2.35				
April–September Parker flow volume	0.36	0.30	0.30	0.31	0.30				
April–September diversion	1.42	1.57	1.56	1.57	1.52				
September 30 reservoir contents	0.04	0.26	0.12	0.27	0.01				
Irrigation proration level	44%	70%	70%	70%	70%				
	<u>1994 dry-year (r</u>	naf <u>)</u>							
April 1 total water supply available (TWSA)	1.74	2.22	2.09	2.01	1.89				
April–September Parker flow volume	0.31	0.25	0.23	0.26	0.25				
April–September diversion	1.23	1.52	1.48	1.44	1.33				
September 30 reservoir contents	0.05	-0.07	-0.12	0.07	-0.15				
Irrigation proration level	21%	70%	68%	56%	48%				
	2001 dry-year (r	naf)							
April 1 total water supply available (TWSA)	1.76	2.45	2.30	2.25	2.23				
April–September Parker flow volume	0.25	0.20	0.19	0.20	0.18				
April–September diversion	1.29	1.55	1.55	1.55	1.51				
September 30 reservoir contents	0.06	0.22	0.07	0.21	0.03				
Irrigation proration level	32%	70%	70%	70%	70%				
	2005 dry-year (r	naf)							
April 1 total water supply available (TWSA)	1.71	2.32	2.16	2.13	2.10				
April–September Parker flow volume	0.25	0.18	0.17	0.19	0.15				
April–September diversion	1.25	1.53	1.53	1.53	1.49				
September 30 reservoir contents	0.08	0.12	-0.02	0.15	-0.04				
Irrigation proration level	28%	70%	70%	70%	70%				

Table 12. Adjusted Integrated Plan Scenario Simulation Results

Shading shows greater than 10% improvement from FWIP conditions, or Prorationing >70%.

Shading shows greater than 10% decrease from FWIP conditions, or Prorationing <70%.

* September 30 reservoir contents do not include 200,000 acre-feet of inactive storage in Kachess that is available in critically dry years under scenarios that include that project.

4.0 Climate Change Impacts Modeling

Hydrologic input for 12 climate change scenarios was provided by Reclamation's Technical Service Center (RMJOC 2010 and RMJOC 2011); six scenarios represented 2020s climate, while the other six represent 2040s climate. An additional seven scenarios were also provided, including six transient-climate scenarios and a historical scenario. The scenarios were developed from climate-specific hydrologic modeling conducted by the University of Washington⁸. Four of the climate-specific scenarios featured in RMJOC's report were selected for incorporation into the Yakima Basin Study's RiverWare models – one to represent historic climate and the others to represent a range of possible future climates.

The historical hydrology dataset, like data for future climates, was based on watershed hydrologic simulation. The remaining three climate scenarios use future hydrologies that portray "hybrid-delta" (HD) climate change, which reflects a shifted envelope of historically based climate variability. The HD scenarios represent climate associated with projected atmospheric and climate conditions that may occur during the 2040s. This "delta" (or change) from historic to 2040 conditions is imposed on 90 years of historically varying hydrologic data (associated with observations during 1917 through 2006). The climate-adjusted hydrologic data from the 1981-2006 sub-period were then used from each of the climate-specific hydrologies (historical and three 2040s scenarios). The three selected HD scenarios represent a "more adverse" (hadgem1), "moderately adverse" (hadcm) and "less adverse" (cgcm3.1 t47) climate change. Table 13 summarizes the historical and the three climate change scenarios.

SCENARIO	CLIMATE MODEL USED	AVERAGE RMJOC LABEL TEMPERATURE CHANGE		AVERAGE PRECIPITATION CHANGE	AVERAGE ANNUAL RESERVOIR INFLOW (ACRE-FEET)
NRNI (Existing or Historical)	Historically Based	None	0	0	1.66 M
Moderately Adverse	HADCM	Central Change (2040s C)	1.7 °C average increase	3.7% increase	1.48 M
Less Adverse	CGCM3.1	None (2040s LW/W)	1.8 °C average increase	13.4% increase	1.86 M
More Adverse	HADGEM1	More Warming, Drier (2040s MW/D)	2.8 °C average increase	2.5% decrease	1.38 M

Table 13. Summary of Climate Change Scenarios

Climate change impacts on hydrology and water demands associated with the three climate scenarios were incorporated into the FWIP and Integrated Plan scenario models by importing the bias-corrected VIC hydrology using the Reclamation's "Daily Bias Correction Calculator" spreadsheet⁹. Irrigation demands were increased by an average of 9 percent to represent climate change-impacted conditions (Water Needs for Out of Stream Uses - Technical Memorandum – Appendix C). M&I demands were increased by an average of 5 percent based on information from the Water Needs Technical Memorandum. The 9 percent increase is based on the Moderately Adverse scenario, but was used in all three climate-influenced scenarios. Because precipitation and evaporation are not simulated in the YAKRW model, there was no way to directly include the effects of climate change on these parameters in the modeling analysis. The demand changes should approximate the influence of temperature and evaporation change on that factor, but no attempt was made to estimate changes in reservoir storage due

⁸ Additional information on the University of Washington's climate change models can be found here: <u>http://www.hydro.washington.edu/2860/</u>

⁹ File "DMI_ManageModelsRuns.xlsm"

to evaporation and precipitation changes. Because the climate change scenarios include both increases in precipitation and increases in temperature (which would increase evaporation), effects on reservoir storage are likely to be somewhat offsetting, and small compared with the flow changes that are incorporated.

In addition to the changes in demands described above, the primary impact of the projected climate changes is on the streamflow at each major reservoir. The climate changes incorporated into each scenario change the volume and timing of flow into the reservoirs and at each diversion location, thereby changing both the need for water from reservoir storage and the ability of the reservoirs to meet those needs. The following three figures (Figures 14 through 16) show how the total of the flow into all five major reservoirs is affected by the projected climate change scenarios.



Figure 14.Comparison of Average Monthly Reservoir Inflows between Historically-based (NRNI) and Moderately Adverse Scenario



Figure 15.Comparison of Average Monthly Reservoir Inflows between Historically-based (NRNI) and More Adverse Scenario



Figure 16.Comparison of Average Monthly Reservoir Inflows between Historically-based (NRNI) and Less Adverse Scenario

4.1 Climate Change Simulation Results

The three climate change scenarios were modeled based on input of the hydrological datasets received from TSC. Results for the three climate change scenarios are summarized in Table 14 below and in the figures and tables in Appendix D.

		lates Disa		lates Disa		lates Disa		
	Moderately	Moderately	(Less	Integ Plan	(More	More		
Resource indicator (measurement)	Adverse)	Adverse	Adverse)	Adverse	Adverse)	Adverse		
· · · · · · · · · · · · · · · · · · ·	HADCM	HADCM	CGSM	CGSM	HADGEM1	HADGEM		
<u>A verage</u>	for water ye	ears 1981–200	05 (maf)		•			
April 1 total water supply available (TWSA)	2.31	2.47	2.64	2.79	1.84	2.02		
April–September Parker flow volume	0.51	0.43	0.60	0.53	0.36	0.30		
April–September diversion	1.51	1.64	1.67	1.79	1.29	1.43		
September 30 reservoir contents	0.08	0.17	0.10	0.39	0.07	0.00		
Irrigation proration level	54%	72%	74%	88%	30%	50%		
	<u>1993 dry-y</u>	/ear (maf)						
April 1 total water supply available (TWSA)	1.86	2.00	2.50	2.65	1.61	1.69		
April–September Parker flow volume	0.38	0.27	0.57	0.57	0.29	0.28		
April–September diversion	1.30	1.46	1.61	1.65	1.16	1.24		
September 30 reservoir contents	0.03	-0.16	0.05	0.25	0.08	-0.17		
Irrigation proration level	30%	52%	58%	70%	7%	23%		
	<u>1994 dry-y</u>	/ear (maf)						
April 1 total water supply available (TWSA)	1.51	1.60	1.73	2.24	1.30	1.43		
April–September Parker flow volume	0.29	0.27	0.25	0.20	0.23	0.21		
April–September diversion	1.10	1.20	1.29	1.56	0.97	1.09		
September 30 reservoir contents	0.08	-0.17	0.05	-0.03	0.10	-0.14		
Irrigation proration level	9%	25%	32%	70%	0%	14%		
	2001 dry-y	/ear (maf)						
April 1 total water supply available (TWSA)	1.58	2.16	1.69	2.26	0.85	1.38		
April–September Parker flow volume	0.33	0.26	0.29	0.22	0.23	0.20		
April–September diversion	1.11	1.49	1.24	1.56	0.53	1.07		
September 30 reservoir contents	0.05	-0.06	0.05	0.00	0.07	-0.17		
Irrigation proration level	9%	61%	25%	70%	0%	10%		
2005 dry-year (maf)								
April 1 total water supply available (TWSA)	1.76	2.02	2.20	2.29	1.48	1.58		
April–September Parker flow volume	0.33	0.26	0.39	0.35	0.30	0.25		
April–September diversion	1.27	1.46	1.56	1.63	1.08	1.16		
September 30 reservoir contents	0.04	-0.12	0.05	0.29	0.07	-0.15		
Irrigation proration level	27%	61%	59%	70%	4%	21%		

Table 14. Climate Change Scenario Simulation Results

Shading shows greater than 10% improvement from FWIP conditions, including effects of climate, or Prorationing >61%.

Shading shows greater than 10% decrease from FWIP conditions, including effects of climate, or Prorationing <61%.

* September 30 reservoir contents do not include 200,000 acre-feet of inactive storage in Kachess that is available in critically dry years under scenarios that include that project.

5.0 Conclusions

The hydrologic simulations described in this technical memorandum provided the technical results necessary for the Workgroup to understand how effectively the proposed Integrated Plan water supply facilities and other changes are able to meet existing and projected water supply needs of the Yakima Basin. The estimates produced by the YAKRW model allow quantified comparison of the following conditions:

- Total water supply available
- Prorationing (the percent of the deliverable supply to the lower-priority water right holders)
- April through September deliveries
- End of September reservoir storage
- Relative success in meeting instream flow target levels

For the Integrated Plan, the model results under existing climate conditions indicate that total water supply available can be increased from an average of 2.79 MAF to 3.00 MAF. During critical drought conditions, total water supply available can be increased from 1.74 MAF to 2.22 MAF. Prorationing levels are increased by the Integrated Plan from an average of 80 percent to an average of 92 percent, and worst critical year prorationing is increased from 21 percent to 70 percent.

Average April through September deliveries are increased from 1.61 MAF to 1.69 MAF, despite projected conservation efforts that reduce demands. Average end of September reservoir storage levels increase under Integrated Plan conditions from 233,000 acre-feet to 577,000 acre-feet. The simulation model indicates improvement in meeting instream flow target objectives in 13 of 14 critical reaches. Hydrographs displaying the reach-by-reach flow improvements are included in Appendix B.

When potential "moderately adverse" climate changes are incorporated into the analysis, similar improvements in water supply and streamflow conditions are estimated when FWIP and Integrated Plan results are compared. In particular, average total water supply available increases from 2.31 MAF to 2.47 MAF. During critical drought conditions, total water supply available is increased from 1.51 MAF to 1.64 MAF.

Prorationing levels are increased by the Integrated Plan under moderately adverse climate impacts from an average of 54 percent to an average of 72 percent, and worst critical year prorationing is increased from 9 percent to 25 percent. Average April through September deliveries are increased from 1.51 MAF to 1.64 MAF, despite projected conservation efforts that reduce demands. End of September reservoir storage levels increase under Integrated Plan moderately adverse climate change conditions from 80,000 acre-feet to 170,000 acre-feet. The simulation model also indicates improvement in meeting instream flow targets objectives. Hydrographs displaying the reach-by-reach flow improvements are included in Appendix B.

6.0 Limitations

This technical memorandum and the hydrologic simulations were completed by HDR to estimate the effectiveness of certain proposed water supply development projects in meeting estimated demands and instream flow targets. The model utilized (YAKRW) was previously developed by Reclamation to describe the operations of the Yakima Basin Project and other facilities and components of the hydrologic system.

The Yakima Basin and the YAKRW model are very complex. Based on engineering judgment and discussion with Reclamation staff and others who have expertise on the Yakima Basin, HDR made

certain changes to the YAKRW model to complete this study. These changes appear to be appropriate, but certain changes could affect results.

The model result summaries presented in this memorandum are accumulations of a large amount of model-simulated results that are affected by assumptions (recognized and unrecognized) that are incorporated into the model and its data files. HDR has exercised a standard level of care in conducting this study that is typical of this level or stage of project planning. However, results should be carefully reviewed for reasonableness prior to using them for decision-making. Results are not appropriate for design-level decision-making. The 2011 RMJOC report¹¹ provides further discussion on the uncertainties of assessing operation impacts in a changing climate (Section 5.0) and the limitations of relating climate projections to hydrologic and operations impacts (Section 6.0).

7.0 References

- 1. Bureau of Reclamation. 2008. "Final Planning Report/Environmental Impact Statement: Yakima River Basin Water Storage Feasibility Study." December 2008.
- Bureau of Reclamation, U.S. Army Corps of Engineers, and Bonneville Power Administration. 2010. Climate and Hydrology Datasets for Use in the RMJOC Agencies' Longer-Term Planning Studies: Part I - Future Climate and Hydrology Datasets (not published). U.S. Department of the Interior, Bureau of Reclamation, Technical Service Center, Denver, Colorado and Pacific Northwest Regional Office, Boise, Idaho; U.S. Army Corps of Engineers, Northwest Division, Portland District, Portland, Oregon; and Bonneville Power Administration, Portland, Oregon. December 2010.
- Bureau of Reclamation. 2011. Climate and Hydrology Datasets for Use in the RMJOC Agencies' Longer-Term Planning Studies: Part II - Reservoir Operations Assessment for Reclamation Tributary Basins (not published). U.S. Department of the Interior, Bureau of Reclamation, Pacific Northwest Regional Office, Boise, Idaho. January 2011.
- 4. Washington State Department of Ecology, "Final Environmental Impact Statement: Yakima River Basin Integrated Water Resource Management Alternative", June 2009.

Name	Background	Responsibility	
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Anchor QEA			
Bob Montgomery	Hydrology	Technical Advisor	

8.0 List of Preparers

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Appendix A –

RiverWare Model Canal Schematics



North Branch Canal:

Groundwater returns from Diversion Groups 1 through 4 to Cascade Canal groundwater system

Surface water returns from Diversion Group No. 1 to Dry Creek

Surface water returns from Diversion Group No. 2 to Reecer Creek

Surface water returns from Diversion Group No. 3 to Wilson Creek

Surface water returns from Diversion Group No. 4 to Cherry Creek

A portion of Wilson Creek is captured by the canal between Diversion groups 2 and 3 South Branch Canal:

Groundwater and Surface water returns from Diversion Group No. 1 to Taneum Creek Groundwater and Surface water returns from Diversion Group No. 2 to Robinson Creek Groundwater and Surface water returns from Diversion Group No. 3 to Manastash Creek





KRD West Side Canal:

Groundwater returns from Diversion Groups 1 through 2 to Yakima alluvium goundwater system

Groundwater returns from Diversion Group No. 3 is consumptively used

Surface water returns from Diversion Group No. 1 to Taneum Creek

Surface water returns from Diversion Group No. 2 to Robinson Creek

Surface water returns from Diversion Group No. 3 to Manastash Creek

A portion of flows from Taneum, Robinson, and Manastash creeks are captured by the canal



Groundwater returns from Diversion Group No. 1 to West Side canal groundwater system Surface water returns from Diversion Group No. 1 to Taneum Creek



<u>\$</u>

Line Break

Notes:

KRD Town Canal:

Groundwater returns from Diversion Groups 1 through 4 to Yakima River alluvium groundwater system Surface water returns from Diversion Group No. 1 to Dry Creek Surface water returns from Diversion Group No. 2 to Reecer Creek

Surface water returns from Diversion Group No. 3 to Wilson Creek

Surface water returns from Diversion Group No. 3 to Cherry Creek

A portion of flows from Dry, Reecer, Wilson, and Cherry creeks are captured by the canal.







Roza Canal Schematic:

Surface water returns from Diversions return to the nearest wasteway.

Groundwater returns from Diversions No. 1 and 2 return to the Selah Moxee groundwater system

Groundwater returns from Diversion No. 3 return to the Union Gap groundwater system

Groundwater returns from Diversions No. 4 to 6 return to the Sunnyside groundwater system





Selah Moxee Canal Schematic:

Surface water returns from Diversions return to the nearest wasteway.

Groundwater returns from Diversion No. 1 return to the Hubbard groundwater system Groundwater returns from Diversion No. 2 return to the Moxee groundwater system

Portions of flow from wasteways 1 and 2 are captured by the canal



Notes:

Moxee Canal Schematic:

Diversion Group No. 2 return flows to Wasteway No. 2 Portions of flow from wasteway 2 are captured by the canal









Reservation Canal Schematic:

Two canal diversions (Old and New canals) from the Yakima River and one pumping (Satus) diversion Diversion groups No. 1 and 2 return flows to Yakima River.



Notes:

Sunnyside Canal Schematic:

Return flows from Diversions are to nearest wasteway.





Chandler and Kennewick Canals Schematic:

All return flows are to Yakima River except for Diversion Group No. 3 which is to Columbia River





Appendix B – Integrated Plan Results

Hydrologic Indicator			Integrated Plan	1			Future w	ithout Integr	ated Plan	
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)						2.79				
April-September flow volume at Parker gage (kaf)	3.00 605	2.22 245	198	2.32 181	4.73 1937	644	1.74 313	1.76 252	1.71 245	4.52 1937
March-October flow volume at Parker gage (kaf)	907	400	2.45 335	310	2638	940	456	377	366	2603
April-September diversion volume upstream of Parker gage (maf)	1.69	1.52	1.55	1.53	1.73	1.61	1.23	1.29	1.25	1.71
September 30 non- Bumping or Wymer reservoir contents (kaf)	348	-121	75	-19	709	218	41	48	62	510
October 31 non- Bumping or Wymer reservoir contents (kaf)	329	-120	74	-26	802	213	65	67	56	619
September 30 Bumping and Wymer reservoir contents (kaf)	229	56	145	144	267	15	7	11	14	18
April-September flow volume at mouth of Yakima River (kaf)	867	349	272	293	2262	888	386	300	333	2245
Irrigation proration level (percent) ¹	92%	70%	70%	70%	100%	80%	21%	32%	28%	100%

Resource indicator		
(measurement)	Integrated Plan	Future without Integrated Plan
	WATER RESOURCES	
	Average for water years 1981–2005 (ma	f)
Water supply April 1 total water supply available (TWSA) Water distribution	3.00	2.79
April–September Parker flow	0.60	0.64
April–September diversion	1.69	1.61
September 30 reservoir contents April–September flow	0.58	0.24
Yakima River	0.87	0.89
	1994 dry-year (maf)	
Water supply April 1 TWSA Water distribution	2.22	1.74
volume	0.25	0.31
April–September diversion September 30 reservoir	1.52	1.23
contents April–September flow	-0.06	0.05
Yakima River	0.35	0.39
Irrigation proration level	70%	21%

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Resource indicator		
(measurement)	Integrated Plan	Future without Integrated Plan
	ANADROMOUS FISH	
Ra	te of change in flow during flip-flop	
(avera	ae cfs/day August 16–September	14)
Easton reach	-7	-21
Ellensburg reach	-45	-103
Lower Naches River reach	31	33
Ρια- (Διι	gust 1-15) and post- (September 1	4-28)
flin-fl	op flow and absolute change in flow	W
Easton reach		
Pre-flip-flop flow (cfs)	574	890
Post-flip-flop flow (cfs)	364	287
Absolute change in flow (cfs)	-211	-603
Ellensburg reach		
Pre-flip-flop flow (cfs)	2,867	4,346
Post-flip-flop flow (cfs)	1,574	1,364
Absolute change in flow (cfs)	-1,293	-2,982
Lower Naches River reach		
Pre-flip-flop flow (cfs)	644	824
Post-flip-flop flow (cfs)	1,548	1,776
Absolute change in flow (cfs)	904	953
Average, minimum, and maximum	reservoir elevation (feet) during	bull trout spawning migration:
Kaabaaa Laka		2220 12 2102 02 2201 02
Nachess Lake	2230.41 2140.99-2201.90	2239.13 2198.U2-2261.96
Neechelus Lake	2410.1 2432.28-2516.96	2400.38 2432.44-2516.88
RIMPOCK LAKE	2914.66 2801.26-2926	2905.93 2846.64-2926

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Item	Future without Integrated Plan	Integrated Plan	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2789.0	3004.9	215.9
gage [kaf]	940.2	906.7	-33.6
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	1740.3	2215.7	475.4
gage [kaf]	456.2	399.8	-56.4
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	1762.1	2453.2	691.1
gage [kaf]	377.4	335.5	-41.9
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	1706.3	2320.8	614.5
gage [kaf]	365.7	310.2	-55.5
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	4517.9	4728.6	210.7
gage [kaf]	2603.3	2638.3	35.0




















Reservoir Storage 11/11/2010



Reservoir Storage 11/11/2010



Reservoir Storage 11/11/2010



















Water Supply Indices 11/11/2010











Appendix C – Adjusted Integrated Plan Results

- C-1 Adjusted Integrated Plan Results without Bumping Reservoir Enlargement
- C-2 Adjusted Integrated Plan Results without Kachess Inactive Storage and Keechelus to Kachess (K to K) Pipeline
- C-3 Adjusted Integrated Plan Results without Wymer Reservoir

Appendix C – 1

Adjusted Integrated Plan Results Without Bumping Reservoir Enlargement

Resource indicator (measurement)	Integrated Plan	Integrated Plan without Bumping Enlargement
	WATER RESOURCES	
	Average for water years 1981–2005 (m	af)
Water supply April 1 total water supply available (TWSA)	3.00	2.96
Water distribution April–September Parker flow	0.60	0.60
April–September diversion September 30 reservoir	1.69	1.69
contents April–September flow volume at mouth of	0.58	0.44
Yakima River	0.87	0.86
	1994 dry-year (maf)	
Water supply		
April 1 TWSA Water distribution April–September Parker flow	2.22	2.09
volume	0.25	0.23
April–September diversion September 30 reservoir	1.52	1.48
contents April–September flow volume at mouth of	-0.06	-0.12
Yakima River	0.35	0.33
Irrigation proration level	70%	68%

Resource indicator		Integrated Plan without Bumping			
(measurement)	Integrated Plan	Enlargement			
	ANADROMOUS FISH				
Poto	of change in flow during flip flop				
naic (average	Of Change in now during inp-nop	11)			
Easton reach	-7	-6			
	-7 -45	-0 -43			
Lower Naches River reach	31				
	.	20			
Pre- (Augı	ust 1-15) and post- (September 1	4-28)			
flip-flor	p flow and absolute change in flow	W			
Easton reach					
Pre-flip-flop flow (cfs)	574	535			
Post-flip-flop flow (cfs)	364	368			
Absolute change in flow (cfs)	-211	-167			
Ellensburg reach					
Pre-flip-flop flow (cfs)	2,867	2,823			
Post-flip-flop flow (cfs)	1,574	1,580			
Absolute change in flow (cfs)	-1,293	-1,244			
Lower Naches River reach					
Pre-flip-flop flow (cfs)	644	748			
Post-flip-flop flow (cfs)	1,548	1,487			
Absolute change in flow (cfs)	904	739			
Average, minimum, and maximum reservoir elevation (feet) during bull trout spawning migration:					
July 15–September 15 (feet)					
Kachess Lake 22	235.41 2146.99-2261.96	2235.67 2145.81-2261.96			
Keechelus Lake 24	476.7 2432.28-2516.96	2476.75 2432.51-2516.96			
Rimrock Lake 29	914.66 2801.26-2926	2912.23 2801.03-2926			

Hydrologic Indicator			Integrated Plar	I		Integ	ırated Plan w	/ithout Bumj	oing Enlarge	ment
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)	3.00	2.22	2.45	2.32	4.73	2.96	2.09	2.30	2.16	4.70
April-September flow volume at Parker gage (kaf)	605	245	198	181	1937	598	226	194	173	1938
March-October flow volume at Parker gage (kaf)	907	400	335	310	2638	901	375	329	301	2637
April-September diversion volume upstream of Parker gage (maf)	1.69	1.52	1.55	1.53	1.73	1.69	1.48	1.55	1.53	1.72
September 30 non- Bumping or Wymer reservoir contents (kaf)	348	-121	75	-19	709	350	-124	51	-49	720
October 31 non- Bumping or Wymer reservoir contents (kaf)	329	-120	74	-26	802	332	-127	51	-54	810
September 30 Bumping and Wymer reservoir contents (kaf)	229	56	145	144	267	83	3	23	24	100
April-September flow volume at mouth of Yakima River (kaf)	867	349	272	293	2262	860	328	269	282	2263
Irrigation proration level (percent) ¹	92%	70%	70%	70%	100%	91%	68%	70%	70%	100%

Item	Integrated Plan without Bumping Enlargement	Integrated Plan	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2958.4	3004.9	46.5
gage [kaf]	901.5	906.7	5.2
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	2086.7	2215.7	129.0
gage [kaf]	374.8	399.8	25.0
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	2303.2	2453.2	150.0
gage [kaf]	329.2	335.5	6.3
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2158.3	2320.8	162.6
gage [kaf]	300.6	310.2	9.6
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	4695.5	4728.6	33.0
gage [kaf]	2637.1	2638.3	1.2





2/1/2002 3/1/2002

4/1/2002

5/1/2002

Date

6/1/2002

7/1/2002

8/1/2002

9/1/2002

10/1/2002

11/1/20

0

11/1/2001 12/1/2001

Slot: Bumping River below Bumping DamGage Outflow

1/1/2002
















River Flow Hydrographs 11/29/2010







Yakima Basin Study PRELIMINARY DRAFT















Water Supply Indices 11/29/2010









Appendix C – 2

Adjusted Integrated Plan Results Without Kachess Inactive Storage and Keechelus to Kachess (K to K) Pipeline

Resource indicator	Integrated Dian	Integrated Plan w/o Kachess				
(measurement)		Inactive and K to K				
WATER RESOURCES						
	Average for water years 1981–2005 (maf))				
Water supply April 1 total water supply available (TWSA)	3.00	3.00				
Water distribution April–September Parker flow	0.00	0.00				
volume	0.60	0.61				
April–September diversion September 30 reservoir	1.69	1.69				
contents April–September flow volume at mouth of	0.58	0.60				
Yakima River	0.87	0.87				
	1994 dry-year (maf)					
Water supply						
April 1 TWSA	2.22	2.01				
Water distribution April–September Parker flow						
volume	0.25	0.26				
April–September diversion September 30 reservoir	1.52	1.44				
contents April–September flow	-0.06	0.07				
volume at mouth of Yakima River	0.35	0.36				
Irrigation proration level	70%	56%				

Resource indicator		Integrated Plan w/o Kachess			
(measurement)	Integrated Plan	Inactive and K to K			
	ANADROMOUS FISH				
Rate	of change in flow during flip-flop				
(averag	e cfs/day August 16–September 1	4)			
Easton reach	-7	-7			
Ellensburg reach	-45	-45			
Lower Naches River reach	31	32			
Pre- (Aug	ust 1-15) and post- (September 14	(-28)			
flin-flo	n flow and absolute change in flow	/			
Faston reach	p new and absolute change in new				
Pre-flip-flop flow (cfs)	574	571			
Post-flip-flop flow (cfs)	364	378			
Absolute change in flow (cfs)	-211	-193			
Ellensburg reach					
Pre-flip-flop flow (cfs)	2,867	2,863			
Post-flip-flop flow (cfs)	1,574	1,568			
Absolute change in flow (cfs)	-1,293	-1,295			
Lower Naches River reach					
Pre-flip-flop flow (cfs)	644	632			
Post-flip-flop flow (cfs)	1,548	1,574			
Absolute change in flow (cfs)	904	942			
Average, minimum, and maximum reservoir elevation (feet) during bull trout spawning migration:					
Vaabaaa Laba	July 15–September 15 (feet)				
Kachess Lake 2	235.41 2146.99-2261.96 2 476 7 2422 28 2516 06	2243.12 2193.96-2262			
Neechelus Lake 2 Dimrock Lake 2	4/0./ 2432.28-2310.90	2407.09 2431.00-2310.99			
	314.00 2001.20-2920	2910.10 2001.00-2920			

Hydrologic Indicator			Integrated Plar	I		Integr	rated Plan w	/o Kachess I	nactive and I	K to K
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)	3.00	2.22	2.45	2.32	4.73	3.00	2.01	2.25	2.13	4.74
April-September flow volume at Parker gage (kaf)	605	245	198	181	1937	609	259	203	187	1947
March-October flow volume at Parker gage (kaf)	907	400	335	310	2638	907	398	340	311	2666
April-September diversion volume upstream of Parker gage (maf)	1.69	1.52	1.55	1.53	1.73	1.69	1.44	1.55	1.53	1.73
September 30 non- Bumping or Wymer reservoir contents (kaf)	348	-121	75	-19	709	366	31	69	35	709
October 31 non- Bumping or Wymer reservoir contents (kaf)	329	-120	74	-26	802	348	61	69	48	803
September 30 Bumping and Wymer reservoir contents (kaf)	229	56	145	144	267	226	37	145	119	267
April-September flow volume at mouth of Yakima River (kaf)	867	349	272	293	2262	871	361	277	301	2273
Irrigation proration level (percent) ¹	92%	70%	70%	70%	100%	91%	56%	70%	70%	100%

Item	Integrated Plan w/o Kachess Inactive and K to K	Integrated Plan	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2996.4	3004.9	8.5
gage [kaf]	906.8	906.7	-0.1
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	2009.9	2215.7	205.8
gage [kaf]	398.4	399.8	1.4
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	2252.4	2453.2	200.8
gage [kaf]	340.4	335.5	
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2125.9	2320.8	195.0
gage [kaf]	311.0	310.2	-0.8
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	4736.6	4728.6	-8.1
gage [kaf]	2666.4	2638.3	-28.1















Average Daily Flow [cfs] 1,500

1,000

500

0

11/1/2001 12/1/2001

Slot: Yakima 202_0 at Easton EASWGage Outflow

1/1/2002

2/1/2002 3/1/2002

7/1/2002

8/1/2002

9/1/2002 10/1/2002

11/1/2002

6/1/2002

5/1/2002

Date

4/1/2002







River Flow Hydrographs 11/29/2010



Yakima Basin Study PRELIMINARY DRAFT



















Water Supply Indices 11/29/2010












Draft Integrated Plan without Kachess Inactive Storage and K to K Pipeline October 28, 2010 Model Run

Appendix C – 3

Adjusted Integrated Plan Results Without Wymer Reservoir

_		
Resource indicator (measurement)	Integrated Plan	Integrated Plan w/o Wymer
	WATER RESOURCES	
	Average for water years 1981–2005 (maf)	
Water supply April 1 total water supply available (TWSA) Water distribution	3.00	2.88
April–September Parker flow volume April–September diversion	0.60 1.69	0.65 1.59
September 30 reservoir contents April–September flow	0.58	0.36
Yakima River	0.87	0.91
	1994 dry-year (maf)	
Water supply April 1 TWSA Water distribution	2.22	1.89
April–September Parker flow volume April–September diversion	0.25 1.52	0.25 1.33
September 30 reservoir contents April–September flow	-0.06	-0.15
volume at mouth of Yakima River	0.35	0.34
Irrigation proration level	70%	48%

Resource indicator		
(measurement)	Integrated Plan	Integrated Plan w/o Wymer
	ANADROMOUS FISH	
Rate	of change in flow during flip-flop	
(average	cfs/day August 16-September 14	4)
Easton reach	-7	-16
Ellensburg reach	-45	-90
Lower Naches River reach	31	18
Pre- (Augus	st 1-15) and post- (September 14	-28)
flip-flop	flow and absolute change in flow	,
Easton reach	· ·	
Pre-flip-flop flow (cfs)	574	820
Post-flip-flop flow (cfs)	364	360
Absolute change in flow (cfs)	-211	-460
Ellensburg reach		
Pre-flip-flop flow (cfs)	2,867	4,154
Post-flip-flop flow (cfs)	1,574	1,557
Absolute change in flow (cfs)	-1,293	-2,597
Lower Naches River reach		
Pre-flip-flop flow (cfs)	644	995
Post-flip-flop flow (cfs)	1,548	1,522
Absolute change in flow (cfs)	904	527
Average, minimum, and maximum re	servoir elevation (feet) during l	oull trout spawning migration:
Ju	uly 15–September 15 (feet)	
Kachess Lake 223	35.41 2146.99-2261.96 2	224.94 2134.41-2261.96
Keechelus Lake 24	76.7 2432.28-2516.96 2	472.59 2432.34-2516.96
Rimrock Lake 29 [°]	14.66 2801.26-2926 2	901.5 2800.7-2926

Г

Hydrologic Indicator	Integrated Plan				Integrated Plan w/o Wymer					
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)	3.00	2.22	2.45	2.32	4.73	2.88	1.89	2.23	2.10	4.62
April-September flow volume at Parker gage (kaf)	605	245	198	181	1937	646	247	176	155	1976
March-October flow volume at Parker gage (kaf)	907	400	335	310	2638	946	395	321	291	2663
April-September diversion volume upstream of Parker gage (maf)	1.69	1.52	1.55	1.53	1.73	1.59	1.33	1.51	1.49	1.65
September 30 non- Bumping or Wymer reservoir contents (kaf)	348	-121	75	-19	709	208	-152	-32	-72	564
October 31 non- Bumping or Wymer reservoir contents (kaf)	329	-120	74	-26	802	199	-139	-27	-76	670
September 30 Bumping and Wymer reservoir contents (kaf)	229	56	145	144	267	144	2	65	29	187
April-September flow volume at mouth of Yakima River (kaf)	867	349	272	293	2262	910	339	249	264	2300
Irrigation proration level (percent) ¹	92%	70%	70%	70%	100%	85%	48%	70%	70%	100%

Item	Integrated Plan w/o Wymer	Integrated Plan	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2877.5	3004.9	127.4
gage [kaf]	946.3	906.7	-39.6
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	1890.7	2215.7	324.9
gage [kaf]	395.4	399.8	4.4
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	2226.8	2453.2	226.4
gage [kaf]	320.9	335.5	14.6
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2098.8	2320.8	222.0
gage [kaf]	291.1	310.2	19.0
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	4622.9	4728.6	105.6
gage [kaf]	2663.0	2638.3	-24.6





4/1/2002

5/1/2002

Date

6/1/2002

7/1/2002

8/1/2002

9/1/2002 10/1/2002 11/1/20

2/1/2002 3/1/2002

200

11/1/2001 12/1/2001 1/1/2002

Slot: Bumping River below Bumping DamGage Outflow













5/1/2002

Date

4/1/2002

1/1/2002

2/1/2002 3/1/2002

0

11/1/2001 12/1/2001

Slot: Yakima 202_0 at Easton EASWGage Outflow

7/1/2002

8/1/2002

9/1/2002 10/1/2002

11/1/2002

6/1/2002











Reservoir Storage 11/29/2010



Reservoir Storage 11/29/2010



Reservoir Storage 11/29/2010













Water Supply Indices 11/29/2010











Appendix D – Climate Change Integrated Plan Results

- D-1 Integrated Plan Results with Climate Change Least Adverse Scenario (CGSM3.1)
- D-2 Integrated Plan Results with Climate Change Moderately Adverse Scenario (HADCM)
- D-3 Integrated Plan Results with Climate Change Moderately Adverse Scenario (HADGEM)

Appendix D –1

Integrated Plan Results with Climate Change Least Adverse Scenario (CGSM3.1)

Resource indicator (measurement)	IP CC Cgsm3.1 70% Proration (least adverse)	FWIP CC Cgsm3.1 70% Proration (least adverse)		
	WATER RESOURCES			
	Average for water years 1981–2005 (maf)			
Water supply April 1 total water supply available (TWSA)	2.79	2.64		
Water distribution April–September Parker flow volume	0.53	0.60		
April–September diversion September 30 reservoir	1.79	1.67		
contents April–September flow volume at mouth of	0.39	0.10		
Yakima River	0.85	0.90		
	1994 dry-year (maf)			
Water supply April 1 TWSA	2.24	1.73		
Water distribution April–September Parker flow				
volume April–September diversion September 30 reservoir	0.20 1.56	0.25 1.29		
contents April–September flow	-0.03	0.06		
volume at mouth of Yakima River	0.39	0.41		
Irrigation proration level	70%	32%		

Resource indicator	IP CC Cgsm3.1 70% Proration	FWIP CC Cgsm3.1 70%
(measurement)	(least adverse)	Proration (least adverse)
	ANADROMOUS FISH	
R	ate of change in flow during flin-flop	
(aver	are of change in now during inp-nop age cfs/day August 16–September 14)
Faston reach	-8	-28
Ellensburg reach	-50	-107
Lower Naches River reach	35	30
	weet 4.45) and next (Dentember 4.4)	
Pre- (Al	Igust 1-15) and post- (September 14-2	28)
Tiip-	nop now and absolute charige in now	
Pre-flin-flop flow (cfs)	575	1 104
Post-flin-flop flow (cfs)	333	294
Absolute change in flow (cfs)	-242	-810
Ellensburg reach		0.0
Pre-flip-flop flow (cfs)	2.969	4.374
Post-flip-flop flow (cfs)	1,519	1,275
Absolute change in flow (cfs)	-1,451	-3,099
Lower Naches River reach		
Pre-flip-flop flow (cfs)	610	883
Post-flip-flop flow (cfs)	1,629	1,743
Absolute change in flow (cfs)	1,019	860
Average, minimum, and maximum	n reservoir elevation (feet) during b	ull trout spawning migration:
	July 15–September 15 (feet)	
Kachess Lake	2225.79 2137.76-2261.05 22	231.2 2197.08-2260.89
Keechelus Lake	2463.71 2430.48-2515.5 24	53.8 2432.26-2513.74
Rimrock Lake	2910.37 2801.09-2925.97 29	000.95 2848.97-2925.76

Hydrologic Indicator	IP	CC Cgsm3.1	70% Proration	(least adver	se)	FWIP	CC Cgsm3.1	70% Prorat	ion (least adv	verse)
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)	2.79	2.24	2.26	2.29	4.27	2.64	1.73	1.69	2.20	4.12
April-September flow volume at Parker gage (kaf)	527	199	220	347	1563	596	245	285	390	1606
March-October flow volume at Parker gage (kaf)	993	469	462	641	2420	1072	513	517	674	2457
April-September diversion volume upstream of Parker gage (maf)	1.79	1.56	1.56	1.63	1.91	1.67	1.29	1.24	1.56	1.87
September 30 non- Bumping or Wymer reservoir contents (kaf)	168	-150	-80	135	525	88	48	43	42	341
October 31 non- Bumping or Wymer reservoir contents (kaf)	140	-141	-71	132	505	90	63	75	47	327
September 30 Bumping and Wymer reservoir contents (kaf)	222	120	81	154	263	11	4	5	5	17
April-September flow volume at mouth of Yakima River (kaf)	852	394	456	651	2075	905	414	497	675	2102
Irrigation proration level (percent) ¹	88%	70%	70%	70%	100%	74%	32%	25%	59%	100%

Item	FWIP CC Cgsm3.1 70% Proration (least adverse)	IP CC Cgsm3.1 70% Proration (least adverse)	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2637.3	2793.5	156.2
gage [kaf]	1072.2	993.0	-79.1
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	1733.9	2237.5	503.6
gage [kaf]	512.7	469.5	-43.2
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	1685.3	2258.4	573.1
gage [kaf]	516.7	462.3	-54.4
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2201.4	2286.0	84.7
gage [kaf]	674.4	640.8	-33.6
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	4119.6	4266.2	146.6
gage [kaf]	2457.3	2420.0	-37.2




























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2/1/2002

3/1/2002

4/1/2002

5/1/2002

Date

6/1/2002

7/1/2002

8/1/2002

9/1/2002

10/1/2002

11/1/2002

1/1/2002

5

11/1/2001 12/1/2001

Slot: Cle Elum River below Cle Elum DamGage Outflow

0

















Reservoir Storage 11/29/2010



Reservoir Storage 11/29/2010





















Water Supply Indices 11/29/2010









70% Proration

(least adverse)

FWIP CC Cgsm3.1 70% Proration

(least adverse)

0.90

Appendix D – 2

Integrated Plan Results with Climate Change Moderately Adverse Scenario (HADCM)

Resource indicator	IP CC HADCM 61% Proration	FWIP CC HADCM 61% Proration				
(measurement)	(moderately adverse)	(moderately adverse)				
WATER RESOURCES						
Д	verage for water years 1981–2005 (m	af)				
Water supply April 1 total water supply						
available (TWSA) Water distribution April–September Parker flow	2.47	2.31				
volume	0.43	0.51				
April–September diversion	1.64	1.51				
September 30 reservoir	0.47					
contents April–September flow	0.17	0.08				
volume at mouth of Yakima River	0.70	0.76				
	1994 dry-year (maf)					
Water supply						
April 1 TWSA	1.60	1.51				
Water distribution April–September Parker flow						
volume	0.27	0.29				
April–September diversion	1.20	1.10				
contents	-0.17	0.08				
April–September flow						
Volume at mouth of Yakima River	0.43	0.42				
Irrigation proration level	25%	9%				

Resource indicator	IP CC HADCM 61% Proration	FWIP CC HADCM 61% Proration				
(measurement)	(moderately adverse)	(moderately adverse)				
	ANADROMOUS FISH	· · · · ·				
	to af all an end in flats all wines flip flat					
Ra	te of change in flow during flip-flop					
Easton roach	ige cis/day August 10–September	14) 2 22				
Ellopshurg roach	-7	-22				
Lower Naches River reach	-40	-90				
Lower Naches River reach	52					
Pre- (Au	Pre- (August 1-15) and post- (September 14-28)					
flip-f	lop flow and absolute change in flo	ow.				
Easton reach						
Pre-flip-flop flow (cfs)	494	903				
Post-flip-flop flow (cfs)	283	252				
Absolute change in flow (cfs)	-210	-651				
Ellensburg reach						
Pre-flip-flop flow (cfs)	2,502	3,757				
Post-flip-flop flow (cfs)	1,104	970				
Absolute change in flow (cfs)	-1,397	-2,787				
Lower Naches River reach						
Pre-flip-flop flow (cfs)	723	654				
Post-flip-flop flow (cfs)	1,660	1,794				
Absolute change in flow (cfs)	937	1,140				
Average, minimum, and maximum reservoir elevation (feet) during bull trout spawning migration:						
	July 15–September 15 (feet)					
Kachess Lake	2186.83 2111.62-2260.82	2225.88 2196.51-2259.86				
Keechelus Lake	2448.53 2428.79-2513.19	2449.3 2430.76-2508.79				
Rimrock Lake	2898.55 2800.95-2925.8	2900.25 2848.38-2926				

Hydrologic Indicator	IP CC	HADCM 61	% Proration (me	oderately adv	verse)	FWIP CC	CHADCM 61	% Proration	(moderately	adverse)
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)						2.31				
April-September flow volume at Parker gage (kaf)	2.47 431	1.60 269	262	2.02 262	3.98 1414	509	1.51 294	1.58 327	1.76 334	3.86 1485
March-October flow volume at Parker gage (kaf)	732	455	2.16 467	505	1881	810	503	527	579	1953
April-September diversion volume upstream of Parker gage (maf)	1.64	1.20	1.49	1.46	1.91	1.51	1.10	1.11	1.27	1.87
September 30 non- Bumping or Wymer reservoir contents (kaf)	12	· -179	-134	-181	401	70	68	45	32	211
October 31 non- Bumping or Wymer reservoir contents (kaf)	1	-145	-136	-170	358	72	63	59	36	186
September 30 Bumping and Wymer reservoir contents (kaf)	156	5	76	61	257	10	11	8	4	16
April-September flow volume at mouth of Yakima River (kaf)	704	428	506	478	2053	761	425	545	524	2107
Irrigation proration level (percent) ¹	72%	, 25%	61%	61%	100%	54%	9%	9%	27%	100%

ltem	FWIP CC HADCM 61%	IP CC HADCM 61% Proration	Improvement
	Proration (moderately adverse)	(moderately adverse)	
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	2314.0	2471.7	157.7
gage [kaf]	810.2	732.0	-78.3
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	1507.5	1598.9	91.4
gage [kaf]	502.7	455.3	-47.3
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	1582.8	2157.4	574.6
gage [kaf]	526.7	466.9	-59.9
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	1758.1	2018.4	260.3
gage [kaf]	579.3	505.0	-74.3
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	3861.4	3981.8	120.4
gage [kaf]	1952.7	1880.6	-72.1







1/1/2002

2/1/2002 3/1/2002

4/1/2002

5/1/2002

Date

0

11/1/2001 12/1/2001

Slot: Naches 16_8 at Naches NACW.Gage Outflow

6/1/2002

7/1/2002

8/1/2002

9/1/2002

10/1/2002

11/1/200







Yakima Basin Study PRELIMINARY DRAFT








































Water Supply Indices 11/29/2010











Appendix D – 3

Integrated Plan Results with Climate Change –Most Adverse Scenario (HADGEM)

Resource indicator (measurement)	IP CC HADGEM 61% Proration (most adverse)	FWIP IP CC HADGEM 61% Proration (most adverse)		
	WATER RESOURCES			
	Average for water years 1981–2005 (maf)			
Water supply April 1 total water supply available (TWSA) Water distribution	2.02	1.84		
April–September Parker flow volume April–September diversion	0.30 1.43	0.36 1.29		
September 30 reservoir contents April–September flow	0.00	0.07		
volume at mouth of Yakima River	0.52	0.55		
	1994 dry-year (maf)			
Water supply April 1 TWSA Water distribution	1.43	1.30		
April–September Parker flow volume April–September diversion	0.21 1.09	0.23 0.97		
September 30 reservoir contents April–September flow	-0.14	0.11		
volume at mouth of Yakima River	0.35	0.34		
Irrigation proration level	14%	0%		

Resource indicator	IP CC HADGEM 61% Proration	FWIP IP CC HADGEM 61%				
(measurement)	(most adverse)	Proration (most adverse)				
	ANADROMOUS FISH					
	Rate of change in flow during flip-flo	ממ				
(av	/erage cfs/dav August 16–Septembe	er 14)				
Easton reach		-9 -27				
Ellensburg reach	-2	24 -74				
Lower Naches River reach		8 41				
Pre-	(August 1-15) and post- (September	- 14-28)				
fl	lip-flop flow and absolute change in f	low				
Easton reach	,					
Pre-flip-flop flow (c	cfs) 57	74 1,007				
Post-flip-flop flow (c	zfs) 29	9 221				
Absolute change in flow (c	zfs) -27	' 4 -786				
Ellensburg reach						
Pre-flip-flop flow (c	cfs) 1,72	2,921				
Post-flip-flop flow (c	ofs) 1,02	.7 787				
Absolute change in flow (c	ofs) -70	-2,134				
Lower Naches River reach						
Pre-flip-flop flow (c	ofs) 92	29 450				
Post-flip-flop flow (c	rfs) 1,17	'1 1,631				
Absolute change in flow (c	ofs) 24	2 1,181				
Average, minimum, and maxim	um reservoir elevation (feet) duri	ng bull trout spawning migration:				
July 15–September 15 (feet)						
Kachess Lake	2163.53 2111.62-2245.06	2219.99 2197.26-2250.44				
Keechelus Lake	2434.72 2427.26-2477.77	2446.56 2431.77-2487.87				
Rimrock Lake	2885.06 2800.91-2925.22	2897.46 2842.34-2924.51				

Hydrologic Indicator	IP (CC HADGEM	61% Proration	(most advei	·se)	FWIP IF	CC HADGE	M 61% Prora	ation (most a	dverse)
	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997	Average 1981-2005	Drought Year 1994	Drought Year 2001	Drought Year 2005	Wet Year 1997
April 1 TWSA (maf)	2.02	1.43	1.38	1.58	2.95	1.84	1.30	0.85	1.48	2.93
April-September flow volume at Parker gage (kaf)	303	208	196	247	876	361	233	227	300	992
March-October flow volume at Parker gage (kaf)	652	468	313	470	1662	720	517	365	541	1759
April-September diversion volume upstream of Parker gage (maf)	1.43	1.09	1.07	1.16	1.80	1.29	0.97	0.53	1.08	1.71
September 30 non- Bumping or Wymer reservoir contents (kaf)	-90	-180	-182	-161	111	61	93	73	60	70
October 31 non- Bumping or Wymer reservoir contents (kaf)	-86	-156	-161	-168	121	56	60	53	49	92
September 30 Bumping and Wymer reservoir contents (kaf)	89	37	15	8	235	9	9	2	10	12
April-September flow volume at mouth of Yakima River (kaf)	518	350	362	481	1274	551	339	338	500	1373
Irrigation proration level (percent) ¹	50%	14%	10%	21%	89%	30%	0%	0%	4%	73%

Item	FWIP IP CC HADGEM 61% Proration (most adverse)	IP CC HADGEM 61% Proration (most adverse)	Improvement
Average 1981-2005			
TWSA [April 1, kaf] March-October flow volume at Parker	1839.3	2017.5	178.2
gage [kaf]	719.7	651.9	-67.7
Drought Year 1994			
TWSA [April 1, kaf] March-October flow volume at Parker	1304.8	1434.0	129.2
gage [kaf]	517.0	468.2	-48.8
Drought Year 2001			
TWSA [April 1, kaf] March-October flow volume at Parker	847.9	1382.7	534.7
gage [kaf]	365.4	313.0	-52.4
Drought Year 2005			
TWSA [April 1, kaf] March-October flow volume at Parker	1477.2	1582.2	105.0
gage [kaf]	541.1	470.0	-71.0
Wet Year 1997			
TWSA [April 1, kaf] March-October flow volume at Parker	2930.6	2953.7	23.2
gage [kaf]	1758.6	1661.6	-97.0



















Draft Integrated Plan Climate Change Results HADGEM1 (most adverse) Scenario October 28, 2010 Model Run



0 2/1/2001 4/1/2001 11/1/2001 11/1/2000 12/1/2000 1/1/2001 3/1/2001 5/1/2001 6/1/2001 7/1/2001 8/1/2001 9/1/2001 10/1/2001 Date Slot: Yakima 202 0 at Easton EASWGage Outflow



Draft Integrated Plan Climate Change Results HADGEM1 (most adverse) Scenario October 28, 2010 Model Run



1/1/2002

2/1/2002

3/1/2002

4/1/2002

5/1/2002

Date

6/1/2002

7/1/2002

8/1/2002

9/1/2002

10/1/2002

11/1/2002

11/1/2001 12/1/2001

Slot: Cle Elum River below Cle Elum DamGage Outflow



Draft Integrated Plan Climate Change Results HADGEM1 (most adverse) Scenario October 28, 2010 Model Run

12/1/2001

11/1/2001

Slot: Yakima 139_8 at Umtanum UMTWGage Outflow

1/1/2002

2/1/2002

3/1/2002

4/1/2002

5/1/2002

Date

6/1/2002

7/1/2002

8/1/2002

9/1/2002

10/1/2002

11/1/20







River Flow Hydrographs 11/29/2010



River Flow Hydrographs 11/29/2010

























Water Supply Indices 11/29/2010







Smaller Canal Deliveries





Draft Integrated Plan Climate Change Results HADGEM1 (most adverse) Scenario October 28, 2010 Model Run